# INTERSECTION EVALUATION STUDY 

Culbreath Road (CR 581) at Ayers/Hayman Road (CR 576)<br>Hernando County

Prepared for:

## HERNANDO COUNTY DEPARTMENT OF PUBLIC WORKS

1525 E. Jefferson St.
Brooksville, FL 34601


Contract for Traffic Operations
Burgess \& Niple Contract No.: \# 18-R00006/PH
Task Work Order: \#16
Continuing Traffic Engineering Services

Prepared by:
Burgess \& Niple, Inc.
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June 2023

## SIGNATURE PAGE

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SIGN / DATE / SEAL

### 1.0 INTRODUCTION

Hernando County Department of Public Works has retained Burgess \& Niple (B\&N) to conduct a Intersection Traffic Analysis at the intersection of Culbreath Road (CR 581) at Ayers/Hayman Road (CR 576) in Hernando County, Florida. As a follow up study of the Traffic Signal Warrant Analysis conducted by B\&N in 2020 (included in Appendix A), this study compares and evaluates the alternatives of traffic signal and roundabout, respectively, for the study intersection. The study has been conducted in accordance with the guidelines and procedures outlined in the FDOT Manual on Uniform Traffic Studies (MUTS), FDOT Design Manual (FDM) and the Manual on Uniform Traffic Control Devices (MUTCD).

Figure 1-1: Project Location Map


### 2.0 EXISTING CONDITION

The intersection of Culbreath Road (CR 581) at Ayers/Hayman Road (CR 576) is located in Hernando County, Florida. Table 2-1 below summarizes the existing conditions at this intersection. Figures 2-1 shows the intersection aerial. Condition Diagram and approach photographs were included in Appendix A.

Table 2-1: Summary of Existing Conditions

| Feature | Description |  |
| :--- | :--- | :--- |
| Major Street | Culbreath Road (CR 581) | Ay |
| Minor Street | Ayers/Hayman Road (CR 576) | Ayers/Hayman Road - 55 MPH |
| Posted Speed Limits | Culbreath Road - 45 MPH | Culbreath Road - Uncontrolled with yellow <br> flashing warning beacon |
| Traffic Control | Ayers/Hayman Road - STOP control <br> supplemented with red flashing beacons |  |

Figure 2-1: Intersection Aerial


### 3.0 TRAFFIC VOLUMES

Volume data and turning movement count (TMC) were collected in the previous study. The intersection TMC indicated a morning peak hour of 7:00 to 8:00 AM and afternoon peak hour of 5:00 to 6:00 PM. It also noted that the heaviest turning movements are the eastbound right turn in the AM peak and the northbound left turn in the PM peak. Detailed count information is included in Appendix A. Future volumes, including Opening Year (2025) and Design Year (2035), were calculated to evaluate the performance of traffic signal and roundabout, respectively. The growth rate of $3 \%$ for all approaches was estimated based on collected volume data and historical AADT from Florida Traffic Online. The projected morning and afternoon peak hour traffic volumes are graphically shown in Figure 3-1 and Figure 3-2 for Opening Year and Design Year, respectively. The Historical AADT reports are included in Appendix B.

Figure 3-1 Opening Year (2025) Peak Hour TMC


Figure 3-2 Design Year (2035) Peak Hour TMC


### 4.0 COLLISION DATA

Crash data for the 3-year period (January 1, 2016 to December 31, 2018) was obtained from the University of Florida's Signal 4 Analytics. A total of 22 crashes were reported within 3 years. Detailed crash analysis and the collision diagram can be found in the previous study in Appendix A.

### 5.0 ALTERNATIVE ANALYSIS

The following alternatives were evaluated as part of this analysis. Concepts can be found for each alternative in Figure 5-1 \& 5-2 on the following pages.

- No Build: Stop controlled intersection with stop signs on the eastbound/westbound approaches.
- Alternative 1: Install traffic signal and add one dedicated left turn lane for all approaches.
- Alternative 2: Construct a one-lane roundabout.


### 5.1 OPERATIONAL IMPACTS

The anticipated opening year for traffic signal and roundabout is 2025, and anticipated design year is 2035. Synchro 11 software and SIDRA 11 were used to analyze operational impacts of all alternatives. Traffic signal plan was optimized via Synchro and HCM $6^{\text {th }}$ Edition model was used for delay and LOS calculation. The operational analysis results were summarized in Table 5-1 for Opening Year (2025) and Future Design Year (2035) traffic volumes using the AM and PM peak hours of $7-8$ AM and 5-6 PM, respectively.

Table 5-1: Summary of Operational Analysis

| Scenarios | Approach | AM |  |  |  |  |  | PM |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | No Build |  | Alternative 1 |  | Alternative 2 |  | No Build |  | Alternative 1 |  | Alternative 2 |  |
|  |  | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS |
| $\begin{aligned} & \text { Opening- } \\ & 2025 \end{aligned}$ | EB | 28 | D | 5 | A | 9 | A | NA* | F | 19 | B | 5 | A |
|  | WB | 28 | D | 10 | A | 4 | A | NA* | F | 28 | C | 9 | A |
|  | NB | 5 | A | 13 | B | 5 | A | 7 | A | 12 | B | 14 | B |
|  | SB | 0 | A | 11 | B | 5 | A | 1 | A | 32 | C | 8 | A |
|  | Overall | 19 | C | 8 | A | 7 | A | NA* | F | 16 | B | 11 | B |
| $\begin{gathered} \text { Design - } \\ 2035 \end{gathered}$ | EB | 112 | F | 9 | A | 14 | B | NA* | F | 31 | C | 6 | A |
|  | WB | 156 | F | 10 | B | 5 | A | NA* | F | 31 | C | 14 | B |
|  | NB | 6 | A | 18 | B | 6 | A | 8 | A | 20 | B | 30 | D |
|  | SB | 0 | A | 14 | B | 6 | A | 0 | A | 38 | D | 11 | B |
|  | Overall | 74 | F | 12 | B | 10 | B | NA* | F | 24 | C | 22 | C |

[^0]The No Build Alternative eastbound and westbound traffic will experience extreme delay (beyond modeled capacity in Synchro) during PM peak hour for both Opening Year (2025) and Design Year (2035) due to the northbound high left turn volumes. The Opening Year (2025) overall delay is 19 second/vehicle (sec/veh) during the AM peak for No Build Alternative, which is expected to worsen to $74 \mathrm{sec} / \mathrm{veh}$ in 2035. Installing a traffic signal and providing dedicated left turn lane for all approaches (Alternative 2) reduces the overall delay and provides acceptable LOS for all scenarios. Compared to the No Build Alternative, the Alternative 2 of roundabout also reduces overall delay for all scenarios and provide the best LOS among the 3 analyzed alternatives. Additional operational information is included in reports in Appendix C. Based on Table 5-1, constructing a roundabout shows the greatest reduction in delay for this intersection.

### 5.2 QUEUE LENGTH ANALYSIS

A turn lane queue length analysis was performed for Alternative 1, utilizing the Design Year (2035) traffic volumes. The total required storage for turn lanes is calculated by summing the max queue and the deceleration length. Max queue lengths ( Q ) were provided by Synchro 11 and deceleration distances were used from FDOT FDM Section 212. For the approaches with low left turning volume and small calculated queue length, the minimum 100 ft queue length is applied as a conservative assumption to accommodate the high truck volume. The shared thru/right turn queue was also shown to determine whether the left turn lane will be impacted. The results of this analysis are shown below in Table 5-2. Additional design analysis will be performed following receipt of design survey to determine the feasibility and impacts of providing left turn lanes. Detailed queue length information is included in reports in Appendix C.

Table 5-2: Summary of Queue Length Analysis

| Lane | NBL | NBT/R | SBL | SBT/R | EBL | EBT/R | WBL | WBT/R |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Decel. Distance (L) |  |  |  |  |  |  |  |  |
| Max Queue Length (Q) | $\mathbf{2}$ | 185 |  | 575 | 100 | 100 |  | 350 |
|  | 125 | 100 | 250 | 350 |  |  |  |  |
| Req'd Storage (Q+L') | 760 | 100 | 285 | 125 | 450 | 250 | 450 | 100 |

Note: ${ }^{1}$ FDOT FDM Exhibit 212-1, 45 MPH Design Speed; L=185', 55 MPH Design Speed; L=350'; ${ }^{2}$ Synchro 11, 95th Percentile Calculated Queue Length, Max AM/PM



### 5.3 BENEFIT COST ANALYSIS

A Benefit Cost Analysis was performed for the 2 proposed alternatives. Based on the USDOT B/C Analysis Guidance for Discretionary Grant Programs (2023), benefits of proposed alternatives comparing to No Build are claimed via delay reduction and safety improvement. Detailed assumptions and data sources are included in Appendix D.

The benefit from reducing delays were calculated by comparing 2025 and 2035 calculated delay (as shown previously in Table 5-1) among alternatives. Daily delay benefits were only derived from AM and PM peak hours per day as a conservative benefit estimate. The Historical Crash Method was used to claim the safety benefits for each alternative. The following Crash Modification Factors (CMFs) were utilized and have been summarized in Table 5-3.

Table 5-3 Crash Modification Factor Summary

| CMF <br> ID | Description | Quality <br> Rating | CMF | Crash <br> Type | Crash <br> Severity | Time <br> of Day | Area <br> Type |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 325 | Conversion of Stop-Controlled <br> Intersection to Signalized Control | 5 stars | 0.56 | All | All | All | Rural |
| 7867 | Conversion of Stop-Controlled <br> Intersection to Roundabout | 3 stars | 0.38 | All | All | All | Not <br> Specified |

Construction costs for the 2 proposed alternatives were estimated and summarized in Table 5-4. Detailed engineer's Estimates for construction cost are included in Appendix D. Impacts of proposed alternatives on right-of-way (ROW) are illustrated in the Concept Plan (Figure 5-1 and 5-2), respectively. At this time, ROW acquisition costs are unknown, only construction costs are included in the analysis.

Table 5-4 Cost Estimates

| Alternative | Construction Cost |
| :---: | :---: |
| Alternative 2: Traffic Signal | $\$ 2,114,467$ |
| Alternative 3: Roundabout | $\$ 2,057,769$ |

The results of the Benefit Cost Analysis were summarized in Table 5-5 and supporting calculations and assumptions are included in Appendix D. Based on this analysis, Alternative 3 of roundabout is preferred for this intersection.

Table 5-5 Benefit Cost Analysis Result Summary

| Alternative | Benefits |  | Costs | Results |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Delay <br> Reduction | Safety |  | Net Present <br> Value | Benefit/Cost <br> Ratio |
| Alternative 2: Traffic Signal | $\$ 689,141$ | $\$ 4,466,244$ | $\$ 2,114,467$ | $\$ 3,169,778$ | 2.6 |
| Alternative 3: Roundabout | $\$ 798,736$ | $\$ 6,293,344$ | $\$ 2,057,769$ | $\$ 5,189,557$ | 3.7 |

### 6.0 RECOMMENDATIONS

Based on the results of the alternative analysis, field observations, and engineering judgment, the following conclusions and recommendations were developed:

- With a Benefit/Cost ratio of 3.7 and net present value of $\$ 5,2$ million dollars, Alternative 2 of roundabout is recommended. However, the final decision should consider the costs of ROW acquisition for the proposed alternatives.


## APPENDIX A

Traffic Signal Warrant Analysis Report

## TRAFFIC SIGNAL WARRANT ANALYSIS

Culbreath Road (CR 581) at Ayers/Hayman Road (CR 576)
Hernando County

Prepared for:

## HERNANDO COUNTY DEPARTMENT OF PUBLIC WORKS

1525 E. Jefferson St.
Brooksville, FL 34601


Contract for Traffic Operations
Burgess \& Niple Contract No.: \# 18-R00006
Task Work Order: \#1
Continuing Traffic Engineering Services

Prepared by:
Burgess \& Niple, Inc.
10006 N. Dale Mabry Hwy, Suite 201
Tampa, FL 33618
June 2020

### 1.0 INTRODUCTION

Hernando County Department of Public Works has retained Burgess \& Niple to conduct a Traffic Signal Warrant Analaysis at the intersection of Culbreath Road (CR 581) at Ayers/Hayman Road (CR 576) in Hernando County, Florida. The intersection is in a rural area of Hernando County. This intersection is a connector eastbound to US 41 by way of Ayers/Hayman Road and to northbound to Brooksville by way of Culbreath Road. The study has been conducted in accordance with the guidelines and procedures outlined in the FDOT Manual on Uniform Traffic Studies (MUTS) and the Manual on Uniform Traffic Control Devices (MUTCD).

Figure 1-1: Project Location Map


### 2.0 EXISTING CONDITIONS

The intersection of Culbreath Road (CR 581) at Ayers/Hayman Road (CR 576) is located in Hernando County, Florida. Table 2-1 below summarizes the existing conditions at this intersection. Figures 2-1 and 2-2 show the intersection aerial and Condition Diagram, respectively. Approach photographs are included in Appendix A.

Table 2-1: Summary of Existing Conditions

| Feature | Description |  |
| :--- | :--- | :--- |
| Major Street | Culbreath Road (CR 581) | Ayers/Hayman Road - 55 MPH |
| Minor Street | Ayers/Hayman Road (CR 576) | A |
| Posted Speed Limits | Culbreath Road - 45 MPH | Culbreath Road - Uncontrolled with yellow <br> flashing warning beacon |
| Traffic Control | Ayers/Hayman Road - STOP control |  |
| supplemented with red flashing beacons |  |  |

Figure 2-1: Intersection Aerial



### 3.0 TRAFFIC VOLUMES

A 24-hour approach count was conducted at the intersection of CR 581 (Culbreath Road) and CR 576 (Ayers/Hayman Road) to determine the 8 peak hours for the turning movement count (TMC). The TMC was conducted on Thursday, February 27, 2020 for the hours of 6:00 to 9:00 AM and 2:00 to 7:00 PM. The 24 -hour approach and TMC summaries are shown in Table 3-1 and Table 3-2, respectively. There were no observed pedestrians or bicyclists during the study period. Detailed count information is included in Appendix B.

Table 3-1: Summary of 24-Hour Approach Counts

| TIME | NB | SB | $\begin{gathered} \text { N/S } \\ \text { TOTAL } \end{gathered}$ | EB | WB | $\begin{gathered} \text { E/W } \\ \text { TOTAL } \end{gathered}$ | GRAND TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12:00 AM | 27 | 1 | 28 | 6 | 2 | 8 | 36 |
| 1:00 AM | 8 | 3 | 11 | 7 | 0 | 7 | 18 |
| 2:00 AM | 13 | 1 | 14 | 5 | 3 | 8 | 22 |
| 3:00 AM | 11 | 4 | 15 | 13 | 2 | 15 | 30 |
| 4:00 AM | 20 | 24 | 44 | 41 | 2 | 43 | 87 |
| 5:00 AM | 48 | 68 | 116 | 173 | 19 | 192 | 308 |
| 6:00 AM | 133 | 123 | 256 | 385 | 47 | 432 | 688 |
| 7:00 AM | 217 | 122 | 339 | 487 | 67 | 554 | 893 |
| 8:00 AM | 203 | 104 | 307 | 308 | 60 | 368 | 675 |
| 9:00 AM | 164 | 72 | 236 | 209 | 50 | 259 | 495 |
| 10:00 AM | 180 | 80 | 260 | 165 | 33 | 198 | 458 |
| 11:00 AM | 190 | 76 | 266 | 139 | 44 | 183 | 449 |
| 12:00 PM | 191 | 74 | 265 | 122 | 48 | 170 | 435 |
| 1:00 PM | 199 | 81 | 280 | 144 | 45 | 189 | 469 |
| 2:00 PM | 277 | 98 | 375 | 157 | 41 | 198 | 573 |
| 3:00 PM | 421 | 84 | 505 | 196 | 45 | 241 | 746 |
| 4:00 PM | 605 | 95 | 700 | 236 | 88 | 324 | 1,024 |
| 5:00 PM | 708 | 85 | 793 | 254 | 79 | 333 | 1,126 |
| 6:00 PM | 442 | 76 | 518 | 166 | 44 | 210 | 728 |
| 7:00 PM | 225 | 37 | 262 | 98 | 17 | 115 | 377 |
| 8:00 PM | 129 | 29 | 158 | 64 | 18 | 82 | 240 |
| 9:00 PM | 128 | 18 | 146 | 44 | 11 | 55 | 201 |
| 10:00 PM | 85 | 16 | 101 | 30 | 7 | 37 | 138 |
| 11:00 PM | 47 | 3 | 50 | 16 | 4 | 20 | 70 |
| TOTAL | 4,671 | 1,374 | 6,045 | 3,465 | 776 | 4,241 | 10,286 |

Table 3-2: Summary of 8-Hour Turning Movement Counts

| TIME | NORTHBOUND |  |  |  |  | SOUTHBOUND |  |  |  |  | EASTBOUND |  |  |  |  | WESTBOUND |  |  |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BEGIN/END | U | L | T | R | TOT | U | L | T | R | TOT | U | L | T | R | TOT | U | L | T | R | TOT | INT |
| 6-7 | 0 | 87 | 43 | 3 | 133 | 0 | 1 | 115 | 7 | 123 | 0 | 0 | 31 | 354 | 385 | 0 | 10 | 34 | 3 | 47 | 688 |
| 7-8 | 0 | 148 | 64 | 5 | 217 | 0 | 3 | 112 | 7 | 122 | 0 | 8 | 46 | 433 | 487 | 0 | 9 | 53 | 5 | 67 | 893 |
| 8-9 | 0 | 128 | 71 | 4 | 203 | 0 | 11 | 78 | 15 | 104 | 0 | 4 | 44 | 260 | 308 | 0 | 10 | 45 | 5 | 60 | 675 |
| 2-3 | 0 | 182 | 89 | 6 | 277 | 0 | 7 | 75 | 16 | 98 | 0 | 17 | 35 | 105 | 157 | 0 | 3 | 34 | 4 | 41 | 573 |
| 3-4 | 0 | 297 | 116 | 8 | 421 | 0 | 5 | 65 | 14 | 84 | 0 | 15 | 32 | 149 | 196 | 0 | 7 | 34 | 4 | 45 | 746 |
| 4-5 | 0 | 453 | 139 | 13 | 605 | 0 | 12 | 74 | 9 | 95 | 0 | 15 | 54 | 167 | 236 | 0 | 7 | 68 | 13 | 88 | 1,024 |
| 5-6 | 0 | 527 | 169 | 12 | 708 | 0 | 5 | 69 | 11 | 85 | 0 | 12 | 48 | 194 | 254 | 0 | 7 | 66 | 6 | 79 | 1,126 |
| 6-7 | 0 | 305 | 131 | 6 | 442 | 0 | 6 | 63 | 7 | 76 | 0 | 11 | 41 | 114 | 166 | 0 | 4 | 38 | 2 | 44 | 728 |
| TOTAL | 0 | 2,127 | 822 | 57 | 3,006 | 0 | 50 | 651 | 86 | 787 | 0 | 82 | 331 | 1,776 | 2,189 | 0 | 57 | 372 | 42 | 471 | 6,453 |
| Percentage | 0\% | 71\% | 27\% | 2\% |  | 0\% | 6\% | 83\% | 11\% |  | 0\% | 4\% | 15\% | 81\% |  | 0\% | 12\% | 79\% | 9\% |  |  |
| Maximum | 0 | 527 | 169 | 13 |  | 0 | 12 | 115 | 16 |  | 0 | 17 | 54 | 433 |  | 0 | 10 | 68 | 13 |  |  |
| Minimum | 0 | 87 | 43 | 3 |  | 0 | 1 | 63 | 7 |  | 0 | 0 | 31 | 105 |  | 0 | 3 | 34 | 2 |  |  |
| -ruck Percentage | 0.0\% | 2.8\% | 2.3\% | 5.3\% | 2.7\% | 0.0\% | 14.0\% | 1.8\% | 2.3\% | 2.7\% | 0.0\% | 2.4\% | 2.1\% | 2.7\% | 2.6\% | 0.0\% | 7.0\% | 3.0\% | 4.8\% | 3.6\% | 2.7\% |

### 4.0 COLLISION DATA

Crash data for the 3-year period (January 1, 2016 to December 31, 2018) was obtained from the University of Florida's Signal 4 Analytics for the intersection of Culbreath Road (CR 581) at Ayers/Hayman Road (CR 576). An overview of the crashes can be found on Table 4-1 and additional details can be found in the Collision Diagram on Figure 4-1.

Table 4-1: Collision Statistics

| Crash Type | $\mathbf{2 0 1 6}$ | $\mathbf{2 0 1 7}$ | $\mathbf{2 0 1 8}$ | Total |
| :--- | :---: | :---: | :---: | :---: |
| Angle | 2 | 7 | 4 | 13 |
| Left Turn | 0 | 0 | 3 | 3 |
| Rear End | 0 | 1 | 2 | 3 |
| Off Road | 0 | 1 | 1 | 2 |
| Animal TOTAL | $\mathbf{2}$ | $\mathbf{9}$ | $\mathbf{1 1}$ | $\mathbf{2 2}$ |
|  | 0 | 0 | 1 | 1 |
| Fatalities | 0 | 0 | 0 | 0 |
| Injuries* | $1(4)$ | $4(10)$ | $5(12)$ | $10(26)$ |
| Day | 2 | 7 | 9 | 18 |
| Night | 0 | 2 | 2 | 4 |
| Wet Conditions | 0 | 1 | 2 | 3 |
| Dry Conditions | 2 | 8 | 9 | 19 |

*Number of injury crashes (Number of injured people)

A total of 22 crashes were reported during the study period. There were no reported fatalities and 10 crashes resulted in 26 injuries. No crashes involving non-motorists were reported. The majority of crashes at this intersection were angle-type crashes, 7 of which occurred during a 12 -month period.


### 5.0 QUALITATIVE ASSESSMENT

Currently, there is are flashing beacons at this 4-way intersection with Ayers/Hayman Road being stop controlled. Sight Obstruction and speeding vehicles have been the most prevalent complaint regarding safety at this intersection.

Request: Numerous requests from citizens and the Hernando County Sheriff's Office (HCSO) have been received regarding the potential for crashes to occur at this intersection.

Operations: General Observations: The following is a brief summary of the observed intersection operations:

- In addition to having stop signs on the right and left sides of the eastbound (EB) and westbound (WB) approaches, there is also an overhead flashing beacon with amber for the northbound (NB) and southbound (SB) approaches and red for EB and WB.
- There are ground-in rumble strips for the east and WB approaches beginning approximately $800-\mathrm{ft}$ upstream of each stop bar. However, the rumble stips only extend for about 300-ft in the EB direction leaving a $500-\mathrm{ft}$ gap immediately upstream of the stop bar with no rumble strips. The WB approach includes rumble strips for the full 800 - ft in advance of the stop bar.
- NB and SB vehicles were observed to arrive at fairly random intervals with minor platooning when large trucks traveled slower than passenger vehicles behind them.
- Very high volume of EB right turns in the morning and NB left turns in the afternoon. The afternoon SB volume is light enough that the NB left turn volume was rarely delayed.
- The site was observed after a rain event and showed signs of ponding at the northeast corner. A crash was actually witnessed during the field review where a vehicle hydroplaned within the intersection and was struck by a second hydroplaning vehicle.
o Although this crash event was witnessed during the field review, wet conditions only accounted for 3 of the 22 crashes.


Disabled vehicle and ponding at northeast corner of intersection

Overall Physical Conditions: In addition to observing operational and safety conditions, correctible physical conditions were also identified. The following observations were made during the field review:

- Physical conditions show no obstructions from any approach. This intesction is in a rural area and visibility is not impeded by alignment, vegetation, or buildings.
- There are no crosswalks at this intersection and no pedestrian traffic was observed.
- Each intersection approach has slightly different signage as can be seen in the Condition Diagram.


### 6.0 SIGNAL WARRANT ANALYSIS

The signal warrant analysis was done in accordance with the procedures and guidelines outlined in the Manual on Uniform Traffic Control Devices (MUTCD 2009) and Manual on Uniform Traffic Studies (MUTS).

For the Signal Warrant Analysis, Culbreath Road is considered the major street and Ayers/Hayman Road. is considered the minor street approach for all the peak hours. Based on the posted speed limit of 45 mph on US 17/92, the 70 percent volume criteria was applied to the analysis. The detailed signal warrant sheets from the MUTCD can be found in Appendix C and Table 6-1 summarizes the results of the warrant analysis. The following additional considerations were included in the analysis:

Table 6-1: Summary of Signal Warrant Analysis

| Warrant | Applicable | Satisfied |  |
| :---: | :--- | :---: | :---: |
| 1 A | Minimum Vehicular Volume | Yes | No |
| $1 B$ | Interruption of Continuous Traffic | No | No |
| 2 | Four Hour Vehicular Volume | Yes | No |
| 3 | Peak Hour | No | No |
| 4 | Pedestrian Volume | Yes | No |
| 5 | School Crossing | No | No |
| 6 | Coordinated Signal System | No | No |
| 7 | Crash Experience | Yes | No |
| 8 | Roadway Network | No | No |
| 9 | Grade Crossing | No |  |

### 7.0 RECOMMENDATIONS

Based on the data collection, field observations, collision analysis, signal warrant analysis, and engineering judgment, the following conclusions and recommendations were developed:

- This intersection does not meet any of the warrants outlined in the MUTCD, therefore, installation of a traffic signal is not recommended.
- Although a wet weather crash was observed during the site visit, based on the 3-year crash history review, only 3 of 22 crashes occurred on wet pavement, therefore, major drainage improvements are not recommended at this time.


## Short Term Improvements

- Consider installing additional rumble stripping along the eastbound approach approximately $\mathbf{1 0 0}^{\prime}$ from the stop bar at 45' spacing to match the westbound approach.
- Consider adjusting the advance warning and route signs per MUTCD standards, as shown on the Improvement Diagram.

Mid Term Improvements

- Consider installing an Intersection Conflict Warning System at the intersection. The system includes warning beacons with TRAFFIC APPROACHING WHEN FLASHING signs along the uncontrolled approaches (CR 581) which are actuated by loops along the stop controlled approaches (CR 576)

Long Term Improvements

- Recommend evaluating the intersection for a roundabout.



## APPENDIX A

Approach Photographs

## Northbound Approach Photograph



Looking north into the intersection along Culbreath Road

## Southbound Approach Photograph



Looking south into the intersection along Culbreath Road

## Eastbound Approach Photograph



Looking east into the intersection along Ayers Road

## Westbound Approach Photograph



Looking west into the intersection along Hayman Road

## APPENDIX B

Traffic Count Data

## ICON Consultant Group, Inc.

10006 N. Dale Mabry Hwy, Suite 201
Tampa, Fl. 33618
(813) 962-8689

Date Start: 2/27/2020
Date End: 2/28/2020
Date Printed: 3/4/2020
Culbreath Rd (Northbound)


## ICON Consultant Group, Inc.

10006 N. Dale Mabry Hwy, Suite 201
Tampa, Fl. 33618
(813) 962-8689

Date Start: 2/27/2020
Date End: 2/28/2020
Date Printed: 3/4/2020 Culbreath Rd (Southbound)


## ICON Consultant Group, Inc.

10006 N. Dale Mabry Hwy, Suite 201
Tampa, Fl. 33618
County: Hernando
Weather: Clear
(813) 962-8689

Date Start: 2/27/2020
Date End: 2/28/2020 Date Printed: 3/4/2020 Ayers Rd (Eastbound)


## ICON Consultant Group, Inc.

10006 N. Dale Mabry Hwy, Suite 201
Tampa, Fl. 33618
(813) 962-8689

Date Start: 2/27/2020
Date End: 2/28/2020 Date Printed: 3/4/2020 Hayman Rd (Westbound)



# /CON Consu/tant Group Inc. 

Culbreath Rd at Ayers Rd /

## Vehicles \& Heavy Vehicles

| Start Time | Culbreath Rd <br> Northbound |  |  |  |  |  | Culbreath Rd Southbound |  |  |  |  |  | Ayers Rd <br> Eastbound |  |  |  |  |  | Hayman Rd <br> Westbound |  |  |  |  |  | $\begin{array}{\|l} \hline \text { Int. } \\ \text { Total } \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { U- } \\ \text { Turn } \end{gathered}$ | LT | TH | RT |  | App. Total | $\begin{gathered} \text { U- } \\ \text { Turn } \\ \hline \end{gathered}$ | LT | TH | RT |  | App. Total | $\begin{gathered} \text { U- } \\ \text { Turn } \end{gathered}$ | LT | TH | RT |  | App. Total | $\begin{aligned} & \text { U- } \\ & \text { Turn } \end{aligned}$ | LT | TH | RT |  | App. <br> Total |  |
| 6:00 AM | 0 | 12 | 10 | 0 | 0 | 22 | 0 | 0 | 23 | 3 | 0 | 26 | 0 | 0 | 3 | 68 | 0 | 71 | 0 | 0 | 6 | 1 | 0 | 7 | 126 |
| 6:15 AM | 0 | 19 | 10 | 1 | 0 | 30 | 0 | 0 | 33 | 0 | 0 | 33 | 0 | 0 | 7 | 96 | 0 | 103 | 0 | 4 | 12 | 0 | 0 | 16 | 182 |
| 6:30 AM | 0 | 24 | 13 | 0 | 0 | 37 | 0 | 1 | 25 | 3 | 0 | 29 | 0 | 0 | 11 | 101 | 0 | 112 | 0 | 3 | 7 | 2 | 0 | 12 | 190 |
| 6:45 AM | 0 | 32 | 10 | 2 | 0 | 44 | 0 | 0 | 34 | 1 | 0 | 35 | 0 | 0 | 10 | 89 | 0 | 99 | 0 | 3 | 9 | 0 | 0 | 12 | 190 |
| Hourly Total | 0 | 87 | 43 | 3 | 0 | 133 | 0 | 1 | 115 | 7 | 0 | 123 | 0 | 0 | 31 | 354 | 0 | 385 | 0 | 10 | 34 | 3 | 0 | 47 | 688 |
| 7:00 AM | 0 | 41 | 13 | 1 | 0 | 55 | 0 | 0 | 25 | 1 | 0 | 26 | 0 | 0 | 6 | 132 | 0 | 138 | 0 | 3 | 17 | 2 | 0 | 22 | 241 |
| 7:15 AM | 0 | 42 | 15 | 2 | 0 | 59 | 0 | 1 | 38 | 1 | 0 | 40 | 0 | 2 | 13 | 102 | 0 | 117 | 0 | 1 | 13 | 3 | 0 | 17 | 233 |
| 7:30 AM | 0 | 38 | 16 | 1 | 0 | 55 | 0 | 1 | 29 | 3 | 0 | 33 | 0 | 2 | 16 | 108 | 0 | 126 | 0 | 2 | 12 | 0 | 0 | 14 | 228 |
| 7:45 AM | 0 | 27 | 20 | 1 | 0 | 48 | 0 | 1 | 20 | 2 | 0 | 23 | 0 | 4 | 11 | 91 | 0 | 106 | 0 | 3 | 11 | 0 | 0 | 14 | 191 |
| Hourly Total | 0 | 148 | 64 | 5 | 0 | 217 | 0 | 3 | 112 | 7 | 0 | 122 | 0 | 8 | 46 | 433 | 0 | 487 | 0 | 9 | 53 | 5 | 0 | 67 | 893 |
| 8:00 AM | 0 | 28 | 17 | 2 | 0 | 47 | 0 | 2 | 21 | 3 | 0 | 26 | 0 | 0 | 11 | 83 | 0 | 94 | 0 | 1 | 12 | 0 | 0 | 13 | 180 |
| 8:15 AM | 0 | 31 | 20 | 1 | 0 | 52 | 0 | 3 | 16 | 4 | 0 | 23 | 0 | 0 | 11 | 67 | 0 | 78 | 0 | 4 | 16 | 1 | 0 | 21 | 174 |
| 8:30 AM | 0 | 38 | 19 | 0 | 0 | 57 | 0 | 2 | 24 | 6 | 0 | 32 | 0 | 2 | 10 | 50 | 0 | 62 | 0 | 2 | 6 | 2 | 0 | 10 | 161 |
| 8:45 AM | 0 | 31 | 15 | 1 | 0 | 47 | 0 | 4 | 17 | 2 | 0 | 23 | 0 | 2 | 12 | 60 | 0 | 74 | 0 | 3 | 11 | 2 | 0 | 16 | 160 |
| Hourly Total | 0 | 128 | 71 | 4 | 0 | 203 | 0 | 11 | 78 | 15 | 0 | 104 | 0 | 4 | 44 | 260 | 0 | 308 | 0 | 10 | 45 | 5 | 0 | 60 | 675 |
|  | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 2:00 PM | 0 | 46 | 20 | 2 | 0 | 68 | 0 | 3 | 18 | 6 | 0 | 27 | 0 | 2 | 12 | 22 | 0 | 36 | 0 | 2 | 10 | 0 | 0 | 12 | 143 |
| 2:15 PM | 0 | 42 | 23 | 1 | 0 | 66 | 0 | 0 | 16 | 1 | 0 | 17 | 0 | 9 | 6 | 21 | 0 | 36 | 0 | 0 | 11 | 0 | 0 | 11 | 130 |
| 2:30 PM | 0 | 42 | 22 | 2 | 0 | 66 | 0 | 3 | 17 | 5 | 0 | 25 | 0 | 5 | 13 | 27 | 0 | 45 | 0 | 0 | 10 | 2 | 0 | 12 | 148 |
| 2:45 PM | 0 | 52 | 24 | 1 | 0 | 77 | 0 | 1 | 24 | 4 | 0 | 29 | 0 | 1 | 4 | 35 | 0 | 40 | 0 | 1 | 3 | 2 | 0 | 6 | 152 |
| Hourly Total | 0 | 182 | 89 | 6 | 0 | 277 | 0 | 7 | 75 | 16 | 0 | 98 | 0 | 17 | 35 | 105 | 0 | 157 | 0 | 3 | 34 | 4 | 0 | 41 | 573 |
| 3:00 PM | 0 | 65 | 15 | 1 | 0 | 81 | 0 | 0 | 18 | 1 | 0 | 19 | 0 | 4 | 9 | 35 | 0 | 48 | 0 | 1 | 12 | 1 | 0 | 14 | 162 |
| 3:15 PM | 0 | 72 | 33 | 1 | 0 | 106 | 0 | 3 | 14 | 2 | 0 | 19 | 0 | 3 | 8 | 39 | 0 | 50 | 0 | 2 | 8 | 0 | 0 | 10 | 185 |
| 3:30 PM | 0 | 71 | 22 | 2 | 0 | 95 | 0 | 1 | 14 | 7 | 0 | 22 | 0 | 4 | 9 | 39 | 0 | 52 | 0 | 0 | 11 | 2 | 0 | 13 | 182 |
| 3:45 PM | 0 | 89 | 46 | 4 | 0 | 139 | 0 | 1 | 19 | 4 | 0 | 24 | 0 | 4 | 6 | 36 | 0 | 46 | 0 | 4 | 3 | 1 | 0 | 8 | 217 |
| Hourly Total | 0 | 297 | 116 | 8 | 0 | 421 | 0 | 5 | 65 | 14 | 0 | 84 | 0 | 15 | 32 | 149 | 0 | 196 | 0 | 7 | 34 | 4 | 0 | 45 | 746 |
| 4:00 PM | 0 | 98 | 29 | 5 | 0 | 132 | 0 | 4 | 25 | 5 | 0 | 34 | 0 | 3 | 10 | 36 | 0 | 49 | 0 | 3 | 10 | 3 | 0 | 16 | 231 |
| 4:15 PM | 0 | 107 | 35 | 2 | 0 | 144 | 0 | 3 | 15 | 1 | 0 | 19 | 0 | 4 | 5 | 43 | 0 | 52 | 0 | 1 | 20 | 3 | 0 | 24 | 239 |
| 4:30 PM | 0 | 132 | 36 | 3 | 0 | 171 | 0 | 3 | 14 | 1 | 0 | 18 | 0 | 3 | 13 | 44 | 0 | 60 | 0 | 1 | 15 | 3 | 0 | 19 | 268 |
| 4:45 PM | 0 | 116 | 39 | 3 | 0 | 158 | 0 | 2 | 20 | 2 | 0 | 24 | 0 | 5 | 26 | 44 | 0 | 75 | 0 | 2 | 23 | 4 | 0 | 29 | 286 |
| Hourly Total | 0 | 453 | 139 | 13 | 0 | 605 | 0 | 12 | 74 | 9 | 0 | 95 | 0 | 15 | 54 | 167 | 0 | 236 | 0 | 7 | 68 | 13 | 0 | 88 | 1024 |
| 5:00 PM | 0 | 123 | 41 | 3 | 0 | 167 | 0 | 0 | 19 | 0 | 0 | 19 | 0 | 3 | 16 | 53 | 0 | 72 | 0 | 2 | 23 | 1 | 0 | 26 | 284 |
| 5:15 PM | 0 | 174 | 48 | 2 | 0 | 224 | 0 | 3 | 20 | 2 | 0 | 25 | 0 | 2 | 7 | 43 | 0 | 52 | 0 | 3 | 18 | 2 | 0 | 23 | 324 |
| 5:30 PM | 0 | 139 | 44 | 2 | 0 | 185 | 0 | 1 | 12 | 6 | 0 | 19 | 0 | 3 | 18 | 50 | 0 | 71 | 0 | 2 | 14 | 2 | 0 | 18 | 293 |
| 5:45 PM | 0 | 91 | 36 | 5 | 0 | 132 | 0 | 1 | 18 | 3 | 0 | 22 | 0 | 4 | 7 | 48 | 0 | 59 | 0 | 0 | 11 | 1 | 0 | 12 | 225 |
| Hourly Total | 0 | 527 | 169 | 12 | 0 | 708 | 0 | 5 | 69 | 11 | 0 | 85 | 0 | 12 | 48 | 194 | 0 | 254 | 0 | 7 | 66 | 6 | 0 | 79 | 1126 |
| 6:00 PM | 0 | 100 | 32 | 1 | 0 | 133 | 0 | 3 | 22 | 2 | 0 | 27 | 0 | 0 | 17 | 50 | 0 | 67 | 0 | 2 | 9 | 0 | 0 | 11 | 238 |
| 6:15 PM | 0 | 94 | 45 | 1 | 0 | 140 | 0 | 1 | 11 | 1 | 0 | 13 | 0 | 6 | 13 | 28 | 0 | 47 | 0 | 2 | 10 | 1 | 0 | 13 | 213 |
| 6:30 PM | 0 | 62 | 30 | 4 | 0 | 96 | 0 | 1 | 15 | 2 | 0 | 18 | 0 | 1 | 9 | 20 | 0 | 30 | 0 | 0 | 8 | 1 | 0 | 9 | 153 |
| 6:45 PM | 0 | 49 | 24 | 0 | 0 | 73 | 0 | 1 | 15 | 2 | 0 | 18 | 0 | 4 | 2 | 16 | 0 | 22 | 0 | 0 | 11 | 0 | 0 | 11 | 124 |
| Hourly Total | 0 | 305 | 131 | 6 | 0 | 442 | 0 | 6 | 63 | 7 | 0 | 76 | 0 | 11 | 41 | 114 | 0 | 166 | 0 | 4 | 38 | 2 | 0 | 44 | 728 |
| Grand Total | 0 | 2127 | 822 | 57 | 0 | 3006 | 0 | 50 | 651 | 86 | 0 | 787 | 0 | 82 | 331 | 1776 | 0 | 2189 | 0 | 57 | 372 | 42 | 0 | 471 | 6453 |
| Approach \% | 0.0 | 70.8 | 27.3 | 1.9 | - | - | 0.0 | 6.4 | 82.7 | 10.9 | - | - | 0.0 | 3.7 | 15.1 | 81.1 | - | - | 0.0 | 12.1 | 79.0 | 8.9 | - | - | - |
| Total \% | 0.0 | 33.0 | 12.7 | 0.9 | - | 46.6 | 0.0 | 0.8 | 10.1 | 1.3 | - | 12.2 | 0.0 | 1.3 | 5.1 | 27.5 | - | 33.9 | 0.0 | 0.9 | 5.8 | 0.7 | - | 7.3 | - |
| Vehicles | 0 | 2068 | 803 | 54 | - | 2925 | 0 | 43 | 639 | 84 | - | 766 | 0 | 80 | 324 | 1728 | - | 2132 | 0 | 53 | 361 | 40 | - | 454 | 6277 |
| \% Vehicles | - | 97.2 | 97.7 | 94.7 | - | 97.3 | - | 86.0 | 98.2 | 97.7 | - | 97.3 | - | 97.6 | 97.9 | 97.3 | - | 97.4 | - | 93.0 | 97.0 | 95.2 | $-$ | 96.4 | 97.3 |
| Heavy Vehicles | 0 | 59 | 19 | 3 | - | 81 | 0 | 7 | 12 | 2 | - | 21 | 0 | 2 | 7 | 48 | - | 57 | 0 | 4 | 11 | 2 | - | 17 | 176 |
| \% Heavy Vehicles | - | 2.8 | 2.3 | 5.3 | - | 2.7 | - | 14.0 | 1.8 | 2.3 | - | 2.7 | - | 2.4 | 2.1 | 2.7 | - | 2.6 | - | 7.0 | 3.0 | 4.8 | - | 3.6 | 2.7 |
| $\begin{gathered} \text { Bicycles on } \\ \text { Road } \\ \hline \end{gathered}$ | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 |
| \% Bicycles on Road | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 |

# ICON Consultant Group Inc. 

Culbreath Rd at Ayers Rd /
Hayman Rd
County: Hernando
Weather: Clear

10006 N. Dale Mabry Suite 201
Tampa, Florida, United States 33618
(813) 962-8689

Count Name: 01_Culbreath Rd at Ayers/ Hayman Rd SWA
Start Date: 02/27/2020
Page No: 1

## Heavy Vehicles

| Start Time | Culbreath Rd <br> Northbound |  |  |  |  |  | Culbreath Rd Southbound |  |  |  |  |  | Ayers Rd <br> Eastbound |  |  |  |  |  | Hayman Rd <br> Westbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \text { U- } \\ \text { Turn } \end{gathered}$ | LT | TH | RT |  | App. Total | $\begin{gathered} \text { U- } \\ \text { Turn } \\ \hline \end{gathered}$ | LT | TH | RT |  | App. <br> Total | $\begin{gathered} \text { U- } \\ \text { Turn } \\ \hline \end{gathered}$ | LT | TH | RT |  | App. Total | $\begin{gathered} \text { U- } \\ \text { Turn } \\ \hline \end{gathered}$ | LT | TH | RT |  | App. Total |  |
| 6:00 AM | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 1 | 5 |
| 6:15 AM | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 |
| 6:30 AM | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Hourly Total | 0 | 1 | 3 | 0 | 0 | 4 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 2 | 0 | 0 | 2 | 12 |
| 7:00 AM | 0 | 1 | 0 | 1 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 7:15 AM | 0 | 2 | 1 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 6 |
| 7:30 AM | 0 | 2 | 2 | 1 | 0 | 5 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 7:45 AM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Hourly Total | 0 | 6 | 3 | 2 | 0 | 11 | 0 | 1 | 2 | 0 | 0 | 3 | 0 | 0 | 0 | 9 | 0 | 9 | 0 | 0 | 1 | 0 | 0 | 1 | 24 |
| 8:00 AM | 0 | 3 | 1 | 0 | 0 | 4 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 8:15 AM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 5 |
| 8:30 AM | 0 | 3 | 2 | 0 | 0 | 5 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 3 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 8:45 AM | 0 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| Hourly Total | 0 | 10 | 3 | 0 | 0 | 13 | 0 | 3 | 2 | 0 | 0 | 5 | 0 | 0 | 1 | 9 | 0 | 10 | 0 | 0 | 1 | 0 | 0 | 1 | 29 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 2:00 PM | 0 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 2:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 2:30 PM | 0 | 2 | 1 | 0 | 0 | 3 | 0 | 1 | 0 | 1 | 0 | 2 | 0 | 1 | 1 | 4 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 2:45 PM | 0 | 4 | 1 | 0 | 0 | 5 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| Hourly Total | 0 | 9 | 2 | 0 | 0 | 11 | 0 | 1 | 3 | 1 | 0 | 5 | 0 | 1 | 1 | 8 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 26 |
| 3:00 PM | 0 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 1 | 6 |
| 3:15 PM | 0 | 1 | 2 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 1 | 7 |
| 3:30 PM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 2 | 0 | 1 | 0 | 2 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 1 | 7 |
| 3:45 PM | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Hourly Total | 0 | 6 | 3 | 0 | 0 | 9 | 0 | 0 | 1 | 1 | 0 | 2 | 0 | 1 | 0 | 8 | 0 | 9 | 0 | 0 | 3 | 0 | 0 | 3 | 23 |
| 4:00 PM | 0 | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 2 | 0 | 3 | 0 | 1 | 0 | 1 | 0 | 2 | 9 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 4:30 PM | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 4 |
| 4:45 PM | 0 | 4 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 3 | 3 | 0 | 6 | 0 | 0 | 0 | 1 | 0 | 1 | 12 |
| Hourly Total | 0 | 8 | 1 | 0 | 0 | 9 | 0 | 2 | 1 | 0 | 0 | 3 | 0 | 0 | 4 | 7 | 0 | 11 | 0 | 1 | 1 | 2 | 0 | 4 | 27 |
| 5:00 PM | 0 | 3 | 0 | 1 | 0 | 4 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 3 | 8 |
| 5:15 PM | 0 | 5 | 2 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 5:30 PM | 0 | 5 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 6 |
| 5:45 PM | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 5 |
| Hourly Total | 0 | 14 | 3 | 1 | 0 | 18 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 2 | 3 | 0 | 0 | 5 | 27 |
| 6:00 PM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 6:15 PM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 3 |
| 6:30 PM | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 6:45 PM | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Hourly Total | 0 | 5 | 1 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 8 |
| Grand Total | 0 | 59 | 19 | 3 | 0 | 81 | 0 | 7 | 12 | 2 | 0 | 21 | 0 | 2 | 7 | 48 | 0 | 57 | 0 | 4 | 11 | 2 | 0 | 17 | 176 |
| Approach \% | 0.0 | 72.8 | 23.5 | 3.7 | - | - | 0.0 | 33.3 | 57.1 | 9.5 | $-$ | - | 0.0 | 3.5 | 12.3 | 84.2 | - | - | 0.0 | 23.5 | 64.7 | 11.8 | - | - | - |
| Total \% | 0.0 | 33.5 | 10.8 | 1.7 | $-$ | 46.0 | 0.0 | 4.0 | 6.8 | 1.1 | - | 11.9 | 0.0 | 1.1 | 4.0 | 27.3 | - | 32.4 | 0.0 | 2.3 | 6.3 | 1.1 | - | 9.7 | - |
| Heavy Vehicles | 0 | 59 | 19 | 3 | - | 81 | 0 | 7 | 12 | 2 | - | 21 | 0 | 2 | 7 | 48 | - | 57 | 0 | 4 | 11 | 2 | - | 17 | 176 |
| \% Heavy Vehicles | - | 100.0 | 100.0 | 100.0 | - | 100.0 | - | 100.0 | 100.0 | 100.0 | - | 100.0 | - | 100.0 | 100.0 | 100.0 | - | 100.0 | - | 100.0 | 100.0 | 100.0 | - | 100.0 | 100.0 |

## Weather: Clear <br> County: Hernando

## Pedestrian / Bicycle Count

Field Data Sheet

File Name: 001_Ped-Bike
Start Date: 2/27/2020
Start Time: 6:00 AM
End Time: 7:00 PM


## APPENDIX C

Signal Warrant Worksheets


## Condition B - Interruption of Continuous Traffic

Condition B is intended for application where Condition A is not satisfied and the traffic volume on a major street is so heavy that traffic on the minor intersecting street suffers excessive delay or conflict in entering or crossing the major street.

| Applicable: | $\square$ Yes | $\square$ No |
| ---: | :---: | :---: |
| 100\% Satisfied: | $\square$ Yes | $\square$ No |
| 80\% Satisfied: | $\square$ Yes | $\square$ No |
| 70\% Satisfied: | $\square$ Yes | $\square$ No |


| Number of traffic on | for moving approach | Vehicles per hour on majorstreet (total of both approaches) |  |  | Vehicles per hour on minorstreet (one direction only) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Major | Minor | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% ${ }^{\text {c }}$ | 100\% ${ }^{\text {a }}$ | 80\% ${ }^{\text {b }}$ | 70\% ${ }^{\text {c }}$ |
| 1 | 1 | 750 | 600 | 525 | 75 | 60 | 53 |
| 2 or more | 1 | 900 | 720 | 630 | 75 | 60 | 53 |
| 2 or more | 2 or more | 900 | 720 | 630 | 100 | 80 | 70 |
| 1 | 2 or more | 750 | 600 | 525 | 100 | 80 | 70 |

${ }^{\text {a }}$ Basic Minimum hourly volume
${ }^{\mathrm{b}}$ Used for combination of Conditions A and B after adequate trial of other remedial measures
${ }^{\text {c }}$ May be used when the major-street speed exceeds 40 mph or in an isolated community with a population of less than 10,000

Record 8 highest hours and the corresponding major-street and minor-street volumes in the Instructions Sheet.

| Eight Highest Hours |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Street | $\sum$ $k$ $k$ $k$ | $\sum$ $\sum$ $\vdots$ $\vdots$ |  | $\sum_{0}$ $\sum_{N}^{M}$ $\sum_{N}^{1}$ | $\sum_{\sum_{n}^{N}}^{\sum_{N}^{+}}$ | $\sum$ <br> $\sum_{0}^{0}$ <br> $\sum_{i}^{1}$ | $\begin{aligned} & \sum_{0}^{2} \\ & \sum_{0}^{0} \\ & \sum_{0}^{1} \end{aligned}$ | $\sum_{0}^{\sum}$ $\sum_{0}^{1}$ 0 |
| Major | 256 | 339 | 307 | 375 | 505 | 700 | 793 | 518 |
| Minor | 44 | 62 | 55 | 52 | 47 | 75 | 73 | 52 |

## Existing Volumes



## Volume Level Criteria

1. Is the posted speed or 85 th-percentile of major street $>40 \mathrm{mph}(70 \mathrm{~km} / \mathrm{h})$ ?

" $70 \%$ " volume level may be used if Question 1 or 2 above is answered "Yes"
$\square 70 \% \square 100 \%$

## WARRANT 3 - PEAK HOUR

If all three criteria are fulfilled or the plotted point lies above the appropriate line, then the warrant is satisfied.

Unusual condition justifying use of warrant:

Record hour when criteria are fulfilled and the corresponding delay or volume in boxes provided.

| Peak Hour 100\% Volume |  |  |
| :---: | :---: | :---: |
| Time | Major Vol. | Minor Vol. |
|  |  |  |

Peak Hour 70\% Volume

| Time | Major Vol. | Minor Vol. |
| :--- | :--- | :--- |
|  |  |  |

## Criteria

| 1. Delay on Minor Approach <br> *(vehicle-hours) |  |  |  |
| :--- | :---: | :---: | :---: |
| Approach Lanes | 1 | 2 |  |
| Delay Criteria* | 4.0 | 5.0 |  |
| Delay* |  |  |  |
| Fulfilled?: |  |  |  |
| Yes |  |  |  |


| 2. Volume on Minor Approach <br> One-Direction *(vehicles per hour) |  |  |  |
| :--- | :---: | :---: | :---: |
| Approach Lanes | 1 | 2 |  |
| Volume Criteria* | 100 | 150 |  |
| Volume* |  |  |  |
| Fulfilled?: | $\square$ | Yes |  |$\square$ No | N |
| :--- |


| 3. Total Intersection Entering <br> Volume **(vehicles per hour) |  |  |  |
| :--- | :---: | :---: | :---: |
| No. of Approaches | 3 | 4 |  |
| Volume Criteria* | 650 | 800 |  |
| Volume* |  |  |  |
| Fulfilled?: | $\square$ | Yes |  |

Plot volume combination on the applicable figure below.


* Note: 150 vph applies as the lower threshold volume for a minor street approach with two or more lanes and 100 vph applies as the lower threshold volume threshold for a minor street approach with one lane.

FIGURE 4C-4: Criteria for "70\%" Volume Level
(Community Less than 10,000 population or above $70 \mathrm{~km} / \mathrm{hr}$ ( 40 mph ) on Major Street)


* Note: 100 vph applies as the lower threshold volume for a minor street approach with two or more lanes and 75 vph applies as the lower threshold volume threshold for a minor street approach with one lane.


# State of Florida Department of Transportation 

## TRAFFIC SIGNAL WARRANT SUMMARY

| City: | NA |
| :---: | :---: |
| County: | 08 - Hernando |
| District: | Seven |
| Major Street: | CR 581 |
| Minor Street: | CR 420 |

Engineer:
Date $\qquad$

| Lanes: | $\mathbf{1}$ | Major Approach Speed: $\quad \mathbf{4 5}$ |
| :--- | :--- | :--- |
| Lanes: | $\mathbf{1} \quad$ Minor Approach Speed: |  |

MUTCD Electronic Reference to Chapter 4: http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf

## Volume Level Criteria

1. Is the posted speed or 85 th-percentile of major street $>40 \mathrm{mph}(70 \mathrm{~km} / \mathrm{h})$ ?
2. Is the intersection in a built-up area of an isolated community with a population $<10,000$ ?

" $70 \%$ " volume level may be used if Question 1 or 2 above is answered "Yes"
$\square 70 \% \quad \square 100 \%$

WARRANT 4 - PEDESTRIAN VOLUME
For each of any 4 hours of an average day, the plotted points lie above the appropriate line, then the warrant is satisfied.

| Applicable: |  |
| ---: | :--- |
| Satisfied: | $\square$ Yes $\square$ No |
| $\square$ No |  |

Plot four volume combinations on the applicable figure below.
Figure 4C-5. Criteria for "100\%" Volume Level

| Four Highest <br> Hours | Volumes |  |
| :--- | :--- | :--- |
|  | Major <br> Street | Pedestrian <br> Total |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |



* Note: 107 pph applies as the lower threshold volume

Figure 4C-6 Criteria for " $70 \%$ " Volume Level


* Note: 75 pph applies as the lower threshold volume


## WARRANT 4 - PEDESTRIAN VOLUME

For 1 hour (any four consecutive 15-minute periods) of an average day, the plotted point falls above the appropriate line, then the warrant is satisfied.

| Applicable: | $\square$ Yes | $\square$ No |
| ---: | :--- | ---: |
| Satisfied: | $\square$ Yes |  |
| $\square$ |  |  |

Plot one volume combination on the applicable figure below.

| $100 \%$ Volume Level |  |  |
| :---: | :---: | :---: |
|  | Volumes |  |
|  | Major <br> Street | Pedestrian <br> Total |
|  |  |  |

Figure 4C-7. Criteria for "100\%" Volume Level - Peak Hour


* Note: 133 pph applies as the lower threshold volume

Figure 4C-8 Criteria for "70\%" Volume Level - Peak Hour


[^1]TRAFFIC SIGNAL WARRANT SUMMARY

| City: | NA |
| :---: | :---: |
| County: | 08 - Hernando |
| District: | Seven |
| Major Street: | CR 581 |
| Minor Street: | CR 420 |

Engineer:
Date:

MUTCD Electronic Reference to Chapter 4: http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf

## WARRANT 5 - SCHOOL CROSSING

Record hours where criteria are fulfilled and the corresponding volume or gap frequency in the boxes provided. The warrant is satisfied if all three of the criteria are fulfilled.

Applicable:Yes $\square$ No
Satisfied:Yes $\square$ No

TRAFFIC SIGNAL WARRANT SUMMARY

| City: | NA | Engineer: Date: | DH |  |
| :---: | :---: | :---: | :---: | :---: |
| County: | 08 - Hernando |  | April 9, 2020 |  |
| District: | Seven |  |  |  |
| Major Street: | CR 581 | Lanes: 1 | Major Approach Speed: | 45 |
| Minor Street: | CR 420 | Lanes: 1 | Minor Approach Speed: | 55 |

MUTCD Electronic Reference to Chapter 4: http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf

## WARRANT 6-COORDINATED SIGNAL SYSTEM

Indicate if the criteria are fulfilled in the boxes provided. The warrant is satisfied if either criterion is fulfilled. This warrant should not be applied when the resulting signal spacing would be less than 300 m (1,000 ft.).

| Applicable: | $\square$ Yes $\quad \checkmark$ No |
| ---: | :--- |
| Satisfied: | $\square$ Yes $\square$ No |


|  | Criteria | Fulfilled? |
| :--- | :---: | :---: |
|  | Yes | No |
| 1. On a one-way street or a street that has traffic predominately in one direction, the adjacent signals are so far <br> apart that they do not provide the necessary degree of vehicle platooning. |  |  |
| 2. On a two-way street, adjacent signals do not provide the necessary degree of platooning, and the proposed <br> and adjacent signals will collectively provide a progressive operation. |  |  |

TRAFFIC SIGNAL WARRANT SUMMARY
Major Street:
Minor Street:
$\square$
Engineer: $\qquad$

| Lanes: $\quad 1 \quad 1$ |
| :--- |
| Lanes: |

Major Approach Speed: $\qquad$

MUTCD Electronic Reference to Chapter 4: http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf

## WARRANT 7 -CRASH EXPERIENCE

Record hours where criteria are fulfilled, the corresponding volume, and other information in the boxes provided. The warrant is satisfied if all three of the criteria are fulfilled.

Applicable:Yes
Satisfied:Yes $\square$ No

| Criteria |  | Hour |  | Volume |  | Met? |  | Fulfilled? |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Major | Minor | Yes | No | Yes |  |
| One of the warrants to the right is met. | Warrant 1, Condition A (80\% satisfied) |  |  |  |  |  |  |  | x |  | x |
|  | Warrant 1, Condition B (80\% satisfied) |  |  |  |  |  | x |  |  |
|  | Warrant 4, Pedestrian Volume at $80 \%$ of volume requirements: \# ped/hr for four (4) hours or \# ped/hr for one (1) hour. |  |  |  |  |  | x |  |  |
| Adequat <br> 2. to reduce | trial of other remedial measure has failed crash frequency. | Measure tried: |  | None |  |  |  |  | x |  |  |
| Five or m <br> 3. to correc month p | re reported crashes, of types susceptible on by signal, have occurred within a 12iod. | Observed <br> Crash <br> Types: | Angle | Number per 12 m | of crash onths: |  | 7 | x |  |  |  |

TRAFFIC SIGNAL WARRANT SUMMARY

| City: | NA |
| ---: | :--- |
| County: |  |
| District: | 08-Hernando |
|  |  |
| Major Street: | Seven |
| Minor Street: |  |


| Engineer: $\quad$ DH |
| ---: |
| Date: |
| April 9, 2020 |

MUTCD Electronic Reference to Chapter 4: http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf

## WARRANT 8 -ROADWAY NETWORK

Record hours where criteria are fulfilled, and the corresponding volume or other information in the boxes provided. The warrant is satisfied if at least one of the criteria is fulfilled and if all intersecting routes have one or more of the Major Route characteristics listed.


| Characteristics of Major Routes |  | Met? |  | Fulfilled? |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Yes | No | Yes | No |
| Part of the street or highway system that serves as the principal roadway <br> 1. network for through traffic flow. | Major Street: |  |  |  |  |
|  | Minor Street: |  |  |  |  |
| 2. Rural or suburban highway outside of, entering, or traversing a city. | Major Street: |  |  |  |  |
|  | Minor Street: |  |  |  |  |
| 3. Appears as a major route on an official plan. | Major Street: |  |  |  |  |
|  | Minor Street: |  |  |  |  |

TRAFFIC SIGNAL WARRANT SUMMARY

| City: | NA |
| :---: | :---: |
| County: | 08 - Hernando |
| District: | Seven |
| Major Street: | CR 581 |
| Minor Street: | CR 420 |



MUTCD Electronic Reference to Chapter 4: http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf

## Approach Lane Criteria

1. How many approach lanes are there at the track crossing?

If there is 1 lane, use Figure $4 \mathrm{C}-9$ and if there are 2 or more, use Figure $4 \mathrm{C}-10$.
$\square 1$ $\begin{array}{ll}1 & \square 2 \\ \text { Fig 4C-9 } & \square \text { Fig }\end{array}$ 2 or Fig 4C-9 Fig 4C-10

## WARRANT 9 - INTERSECTION NEAR A GRADE CROSSING

This signal warrant should be applied only after adequate consideration has been given to other alternatives or after a trial of an alternative has failed to alleviate the safety concerns associated with the grade crossing.
Indicate if both criteria are fulfilled in the boxes provided. The warrant is satisfied if both criteria are met.

| Applicable: | $\square$ Yes | $\square$ No |
| ---: | :--- | :--- |
| Satisfied: | $\square$ Yes | $\square$ No |


| Criteria | Fulfilled? |  |
| :--- | :---: | :---: |
|  | Yes | No |
| 1. A grade crossing exists on an approach controlled by a STOP or YIELD sign and the center of the track nearest to the <br> intersection is within 140 feet of the stop line or yield line on the approach; and | $\square$ | $\square$ |
| 2. During the highest traffic volume hour during which the rail uses the crossing, the plotted point falls above the applicable <br> curve for the existing combination of approach lanes over the track and the distance D (clear storage distance). | $\square$ | $\square$ |

Use the following tables (4C-2, 4C-3, and 4C-4 to appropriately adjust the minor-street approach volume).

## Inputs

Occurrences of Rail traffic per day
\% of High Occupancy Buses on Minor-Street Approach
Enter D (feet)
\% of Tractor-Trailer Trucks on Minor-Street Approach
Adjustment Factors from Tables


Table 4C-2. Adjustment Factor for Daily Frequency of Rail Traffic

Table 4C-3. Adjustment Factor for Percentage of High-

| Rail Traffic |  |
| :---: | :---: |
| Rail Traffic per Day | Adjustment Factor |
| 1 | 0.67 |
| 2 | 0.91 |
| 3 to 5 | 1.00 |
| 6 to 8 | 1.18 |
| 9 to 11 | 1.25 |
| 12 or more | 1.33 |

Occupancy Buses

| \% of High-Occupancy Buses* on <br> Minor Street Approach | Adjustment Factor |
| :---: | :---: |
| $0 \%$ | 1.00 |
| $2 \%$ | 1.09 |
| $4 \%$ | 1.19 |
| $6 \%$ or more |  |
| ${ }^{\text {* }}$ A high-occupancy bus is defined as a bus occupied by at least 20 people |  |

Table 4C-4. Adjustment Factor for Percentage of Tractor-Trailer Trucks

| \% of Tractor-Trailer Trucks on Minor- <br> Street Approach | Adjustment Factor |  |
| :---: | :---: | :---: |
|  | D less than 70 feet | D of 70 feet or more |
| $0 \%$ to $2.5 \%$ | 0.50 | 0.50 |
| $2.6 \%$ to $7.5 \%$ | 0.75 | 0.75 |
| $7.6 \%$ to $12.5 \%$ | 1.00 | 1.00 |
| $12.6 \%$ to $17.5 \%$ | 2.30 | 1.15 |
| $17.6 \%$ to $22.5 \%$ | 2.70 | 1.35 |
| $22.6 \%$ to $27.5 \%$ | 3.28 | 1.64 |
| More than $27.5 \%$ | 4.18 | 2.09 |



TRAFFIC SIGNAL WARRANT SUMMARY

| City: | NA | Engineer: Date: | DH |  |
| :---: | :---: | :---: | :---: | :---: |
| County: | 08 - Hernando |  | April 9, 2020 |  |
| District: | Seven |  |  |  |
| Major Street: | CR 581 | Lanes: 1 | Major Approach Speed: | 45 |
| Minor Street: | CR 420 | Lanes: 1 | Minor Approach Speed: | 55 |

MUTCD Electronic Reference to Chapter 4: http://mutcd.fhwa.dot.gov/pdfs/2009r1r2/part4.pdf

## CONCLUSIONS

Remarks: $\qquad$

WARRANTS SATISFIED:

| \| | Warrant 1 | \| | Not Applicable |
| :---: | :---: |
| $\square$ Warrant 2 | $\square$ Not Applicable |
| \| | Warrant 3 | \| $V$ Not Applicable |
| $\square$ Warrant 4 | $\square$ Not Applicable |
| \| I Warrant 5 | \| $V$ Not Applicable |
| \| I Warrant 6 | \| $/$ Not Applicable |
| $\square$ Warrant 7 | $\square$ Not Applicable |
| \| | Warrant 8 | \| $V$ Not Applicable |
| $\square$ Warrant 9 | $\checkmark$ Not Applicable |

## APPENDIX B

Historical AADT Reports

COUNTY: 08 - HERNANDO
SITE: 9018 - AYERS RD, E OF US41/BROAD ST

| YEAR | AAD T |  | DIRECTION 1 |  | DIRECTION 2 |  | *K FACTOR | D FACTOR | T FACTOR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2022 | 7700 | C | E | 3700 | W | 4000 | 9.50 | 54.50 | 6.50 |
| 2021 | 7500 | C | E | 3500 | W | 4000 | 9.50 | 54.20 | 4.70 |
| 2020 | 4000 | X |  | 0 |  | 0 | 9.50 | 54.30 | 4.50 |
| 2019 | 4100 | X |  | 0 |  | 0 | 9.50 | 54.30 | 4.50 |
| 2018 | 4000 | X |  | 0 |  | 0 | 9.50 | 54.40 | 13.80 |
| 2017 | 3900 | 6 |  | 0 |  | 0 | 9.50 | 55.60 | 6.70 |
| 2016 | 3700 | V |  | 0 |  | 0 | 9.50 | 54.80 | 11.80 |
| 2015 | 3500 | R |  | 0 |  | 0 | 9.50 | 55.00 | 13.20 |
| 2014 | 3300 | T |  |  |  |  | 9.50 | 56.00 | 10.70 |
| 2013 | 3300 | S |  | 0 |  | 0 | 9.50 | 57.60 | 13.30 |
| 2012 | 3300 | F |  | 0 |  | 0 | 9.50 | 55.00 | 12.10 |
| 2011 | 3300 | C | E | 0 | W | 0 | 9.50 | 55.00 | 12.40 |

AADT FLAGS: $C=$ COMPUTED; E = MANUAL ESTIMATE; F = FIRST YEAR ESTIMATE
$S=$ SECOND YEAR ESTIMATE; $T=$ THIRD YEAR ESTIMATE; R = FOURTH YEAR ESTIMATE $\begin{array}{ll}S & =\text { SECOND YEAR ESTIMATE; } \mathrm{T}=\text { THIRD YEAR ESTIMATE; R }=\text { FOURH } \\ \mathrm{V}=\mathrm{FIFTH} \text { YEAR ESTIMATE; } 6=\text { SIXTH YEAR ESTIMATE; X }=\text { UNKNOWN }\end{array}$
*K FACTOR: STARTING WITH YEAR 2011 IS STANDARDK, PRIOR YEARS ARE K30 VALUES

COUNTY: 08 - HERNANDO
SITE: 9607 - CR 581, BETWEEN 'CR 576' AND 'ENDSLEY RD'

| YEAR | AADT | DIRECTION 1 |  |  | CTION | *K FACTOR | D FACTOR | T FACTOR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2022 | 3400 F | N | 1800 | S | 1600 | 9.50 | 54.50 | 6.50 |
| 2021 | 3200 C | N | 1700 | S | 1500 | 9.50 | 54.20 | 4.70 |

AADT FLAGS: $C=$ COMPUTED; E = MANUAL ESTIMATE; F = FIRST YEAR ESTIMATE
$S=$ SECOND YEAR ESTIMATE; $T=$ THIRD YEAR ESTIMATE; R = FOURTH YEAR ESTIMATE $\mathrm{V}=\mathrm{FIFTH}$ YEAR ESTIMATE; $6=$ SIXTH YEAR ESTIMATE; $\mathrm{X}=$ UNKNOWN
*K FACTOR: STARTING WITH YEAR 2011 IS STANDARDK, PRIOR YEARS ARE K30 VALUES

COUNTY: 08 - HERNANDO
SITE: 9624 - CR 572 B/W EMERSON RD AND CULBREATH RD

| YEAR | AADT |  | DIRECTION 1 |  | DIRECTION 2 |  | *K FACTOR | D FACTOR | T FACTOR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2022 | 4300 | F | E | 2200 | W | 2100 | 9.50 | 54.50 | 11.20 |
| 2021 | 4100 | C | E | 2100 | W | 2000 | 9.50 | 54.20 | 6.10 |

AADT FLAGS: $C=$ COMPUTED; E = MANUAL ESTIMATE; F = FIRST YEAR ESTIMATE
$S=$ SECOND YEAR ESTIMATE; T = THIRD YEAR ESTIMATE; R = FOURTH YEAR ESTIMATE $\mathrm{V}=\mathrm{FIFTH}$ YEAR ESTIMATE; $6=$ SIXTH YEAR ESTIMATE; X $=$ UNKNOWN
*K FACTOR: STARTING WITH YEAR 2011 IS STANDARDK, PRIOR YEARS ARE K30 VALUES

## APPENDIX C

Operational Analysis Reports
(Synchro and Sidra)

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 18.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | ${ }_{\dagger}$ |  |  | ${ }_{4}$ |  |  | ${ }_{4}$ |  |  | ${ }_{\dagger}$ |  |  |
| Traffic Vol, veh/h | 9 | 53 | 498 | 10 | 61 | 6 | 170 | 74 | 6 | 3 | 129 | 8 |  |
| Future Vol, veh/h | 9 | 53 | 498 | 10 | 61 | 6 | 170 | 74 | 6 | 3 | 129 | 8 |  |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | - |  | None | - | - | None | - | - | None | - |  | None |  |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |  |
| Mumt Flow | 10 | 59 | 552 | 11 | 68 | 7 | 188 | 82 | 7 | 3 | 143 | 9 |  |





HCM LOS

| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1 | SBL | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1490 | - | - | - | -1337 | - | - |
| HCM Lane V/C Ratio | 0.451 | - | - | - | -0.005 | - | - |
| HCM Control Delay (s) | 9.4 | 0 | - | - | - | 7.7 | 0 |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds $300 \mathrm{~s} \quad+$ : Computation Not Defined *: All major volume in platoon



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 5.1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | ${ }^{\text {¢ }}$ |  |  | $\dagger$ |  |  | ¢ |  |  | ${ }^{4}$ |  |  |
| Traffic Vol, veh/h | 17 | 70 | 281 | 10 | 96 | 9 | 764 | 245 | 17 | 7 | 100 | 16 |  |
| Future Vol, veh/h | 17 | 70 | 281 | 10 | 96 | 9 | 764 | 245 | 17 | 7 | 100 | 16 |  |
| Conflicting Peds, \#hhr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - |  | None |  |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| Mumt Flow | 19 | 78 | 312 | 11 | 106 | 10 | 847 | 272 | 19 | 8 | 111 | 18 |  |



HCM LOS

| Minor Lane/Major Mvmt | NBL | NBT | NBR EBLn1WBLn1 | SBL | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1457 | - | - | - | -1271 | - | - |
| HCM Lane V/C Ratio | 0.581 | - | - | - | -0.006 | - | - |
| HCM Control Delay (s) | 10.8 | 0 | - | - | - | 7.8 | 0 |
| - |  |  |  |  |  |  |  |
| HCM Lane LOS | B | A | - | - | - | A | A |
| HCM 95th \%tile Q(veh) | 4 | - | - | - | - | 0 | - |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds $300 \mathrm{~s} \quad+$ : Computation Not Defined *: All major volume in platoon

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\dagger$ |  | ${ }^{1 /}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{*}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 9 | 53 | 498 | 10 | 61 | 6 | 170 | 74 | 6 | 3 | 129 | 8 |
| Future Volume (vph) | 9 | 53 | 498 | 10 | 61 | 6 | 170 | 74 | 6 | 3 | 129 | 8 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.864 |  |  | 0.986 |  |  | 0.988 |  |  | 0.991 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1752 | 1594 | 0 | 1752 | 1819 | 0 | 1752 | 1823 | 0 | 1752 | 1828 | 0 |
| Flt Permitted | 0.708 |  |  | 0.388 |  |  | 0.660 |  |  | 0.699 |  |  |
| Satd. Flow (perm) | 1306 | 1594 | 0 | 716 | 1819 | 0 | 1217 | 1823 | 0 | 1289 | 1828 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 552 |  |  | 7 |  |  | 7 |  |  | 7 |  |
| Link Speed (mph) |  | 55 |  |  | 55 |  |  | 45 |  |  | 45 |  |
| Link Distance (ft) |  | 977 |  |  | 1082 |  |  | 1598 |  |  | 1480 |  |
| Travel Time (s) |  | 12.1 |  |  | 13.4 |  |  | 24.2 |  |  | 22.4 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% |
| Heavy Vehicles (\%) | 3\% | 3\% | 3\% | 3\% | 3\% | 3\% | 3\% | 3\% | 3\% | 3\% | 3\% | 3\% |
| Adj. Flow (vph) | 10 | 59 | 552 | 11 | 68 | 7 | 188 | 82 | 7 | 3 | 143 | 9 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 10 | 611 | 0 | 11 | 75 | 0 | 188 | 89 | 0 | 3 | 152 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(ft) |  | 12 |  |  | 12 |  |  | 12 |  |  | 12 |  |
| Link Offset(ft) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(ft) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 |  | 1 | 2 |  | 1 | 2 |  | 1 | 2 |  |
| Detector Template | Left | Thru |  | Left | Thru |  | Left | Thru |  | Left | Thru |  |
| Leading Detector (ft) | 20 | 100 |  | 20 | 100 |  | 20 | 100 |  | 20 | 100 |  |
| Trailing Detector (ft) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Position(ft) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Size(ft) | 20 | 6 |  | 20 | 6 |  | 20 | 6 |  | 20 | 6 |  |
| Detector 1 Type | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |  | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ |  | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |  | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex |  |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 1 Queue (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 1 Delay (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 2 Position(ft) |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size(ft) |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | $\mathrm{Cl}+\mathrm{Ex}$ |  |  | $\mathrm{Cl}+\mathrm{Ex}$ |  |  | $\mathrm{Cl}+\mathrm{Ex}$ |  |  | $\mathrm{Cl}+\mathrm{Ex}$ |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 |  |


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| Minimum Split (s) | 23.5 | 23.5 |  | 23.5 | 23.5 |  | 22.8 | 22.8 |  | 22.8 | 22.8 |  |
| Total Split (s) | 26.0 | 26.0 |  | 26.0 | 26.0 |  | 24.0 | 24.0 |  | 24.0 | 24.0 |  |
| Total Split (\%) | 52.0\% | 52.0\% |  | 52.0\% | 52.0\% |  | 48.0\% | 48.0\% |  | 48.0\% | 48.0\% |  |
| Maximum Green (s) | 18.5 | 18.5 |  | 18.5 | 18.5 |  | 17.2 | 17.2 |  | 17.2 | 17.2 |  |
| Yellow Time (s) | 5.5 | 5.5 |  | 5.5 | 5.5 |  | 4.8 | 4.8 |  | 4.8 | 4.8 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 7.5 | 7.5 |  | 7.5 | 7.5 |  | 6.8 | 6.8 |  | 6.8 | 6.8 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | None | None |  | None | None |  |
| Act Effct Green (s) | 14.1 | 14.1 |  | 14.1 | 14.1 |  | 11.2 | 11.2 |  | 11.1 | 11.1 |  |
| Actuated g/C Ratio | 0.43 | 0.43 |  | 0.43 | 0.43 |  | 0.34 | 0.34 |  | 0.34 | 0.34 |  |
| v/c Ratio | 0.02 | 0.61 |  | 0.04 | 0.10 |  | 0.45 | 0.14 |  | 0.01 | 0.24 |  |
| Control Delay | 10.0 | 5.2 |  | 10.4 | 9.7 |  | 15.0 | 10.0 |  | 10.0 | 11.0 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 10.0 | 5.2 |  | 10.4 | 9.7 |  | 15.0 | 10.0 |  | 10.0 | 11.0 |  |
| LOS | A | A |  | B | A |  | B | B |  | A | B |  |
| Approach Delay |  | 5.3 |  |  | 9.8 |  |  | 13.4 |  |  | 11.0 |  |
| Approach LOS |  | A |  |  | A |  |  | B |  |  | B |  |
| Queue Length 50th (ft) | 1 | 8 |  | 1 | 9 |  | 26 | 10 |  | 0 | 18 |  |
| Queue Length 95th (ft) | 9 | 69 |  | 10 | 33 |  | 88 | 40 |  | 5 | 63 |  |
| Internal Link Dist (ft) |  | 897 |  |  | 1002 |  |  | 1518 |  |  | 1400 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 798 | 1188 |  | 437 | 1114 |  | 708 | 1064 |  | 750 | 1066 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.01 | 0.51 |  | 0.03 | 0.07 |  | 0.27 | 0.08 |  | 0.00 | 0.14 |  |

隹section Summary
Area Type:

## Other

Cycle Length: 50
Actuated Cycle Length: 32.8
Natural Cycle: 50
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.61
Intersection Signal Delay: 8.4
Intersection LOS: A
Intersection Capacity Utilization 68.8\%
ICU Level of Service C
Analysis Period (min) 15
Splits and Phases: 3:


Ayres at Culbreath AM _2025
Synchro 11 Report
Page 2

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | F |  | \% | ${ }_{7}$ |  | \% | $\hat{\square}$ |  | \% | ${ }_{7}$ |  |
| Traffic Volume (vph) | 14 | 55 | 223 | 8 | 76 | 7 | 606 | 194 | 14 | 6 | 79 | 13 |
| Future Volume (vph) | 14 | 55 | 223 | 8 | 76 | 7 | 606 | 194 | 14 | 6 | 79 | 13 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.880 |  |  | 0.987 |  |  | 0.990 |  |  | 0.979 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1770 | 1639 | 0 | 1770 | 1839 | 0 | 1770 | 1844 | 0 | 1770 | 1824 | 0 |
| Flt Permitted | 0.697 |  |  | 0.395 |  |  | 0.418 |  |  | 0.615 |  |  |
| Satd. Flow (perm) | 1298 | 1639 | 0 | 736 | 1839 | 0 | 779 | 1844 | 0 | 1146 | 1824 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 207 |  |  | 5 |  |  | 8 |  |  | 8 |  |
| Link Speed (mph) |  | 55 |  |  | 55 |  |  | 45 |  |  | 45 |  |
| Link Distance (t) |  | 977 |  |  | 1082 |  |  | 1598 |  |  | 1480 |  |
| Travel Time (s) |  | 12.1 |  |  | 13.4 |  |  | 24.2 |  |  | 22.4 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% |
| Adj. Flow (vph) | 16 | 61 | 247 | 9 | 84 | 8 | 672 | 215 | 16 | 7 | 88 | 14 |


| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group Flow (vph) | 16 | 308 | 0 | 9 | 92 | 0 | 672 | 231 | 0 | 7 | 102 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(t) |  | 12 |  |  | 12 |  |  | 12 |  |  | 12 |  |
| Link Offset(ft) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(tt) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 |  | 1 | 2 |  | 1 | 2 |  | 1 | 2 |  |
| Detector Template | Left | Thru |  | Left | Thru |  | Left | Thru |  | Left | Thru |  |
| Leading Detector (tt) | 20 | 100 |  | 20 | 100 |  | 20 | 100 |  | 20 | 100 |  |
| Trailing Detector (tt) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Position(tt) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Size(ft) | 20 | 6 |  | 20 | 6 |  | 20 | 6 |  | 20 | 6 |  |
| Detector 1 Type | Cl+Ex | Cl+Ex |  | Cl+Ex | Cl+Ex |  | Cl+Ex | Cl+Ex |  | Cl+Ex | Cl+Ex |  |


| Detector 1 Channel |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(tt) |  | 94 |  | 94 |  | 94 |  | 94 |
| Detector 2 Size(ft) |  | 6 |  | 6 |  | 6 |  | 6 |
| Detector 2 Type |  | Cl+Ex |  | Cl+Ex |  | Cl+Ex |  | Cl+Ex |

Detector 2 Channel

| Detector 2 Extend (s) |  | 0.0 |  | 0.0 |  | 0.0 |  | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Turn Type | Perm | NA | Perm | NA | pm+pt | NA | Perm | NA |
| Protected Phases |  | 4 |  | 8 | 5 | 2 | 6 | 6 |
| Permitted Phases | 4 |  | 8 |  | 2 |  | 0 | 6 |
| Detector Phase | 4 | 4 | 8 | 8 | 5 | 2 | 6 |  |

Switch Phase

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum Initial (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 5.0 | 4.0 |  | 4.0 | 4.0 |  |
| Minimum Split (s) | 23.5 | 23.5 |  | 23.5 | 23.5 |  | 9.5 | 22.8 |  | 22.8 | 22.8 |  |
| Total Split (s) | 27.0 | 27.0 |  | 27.0 | 27.0 |  | 38.0 | 63.0 |  | 25.0 | 25.0 |  |
| Total Split (\%) | 30.0\% | 30.0\% |  | 30.0\% | 30.0\% |  | 42.2\% | 70.0\% |  | 27.8\% | 27.8\% |  |
| Maximum Green (s) | 19.5 | 19.5 |  | 19.5 | 19.5 |  | 33.5 | 56.2 |  | 18.2 | 18.2 |  |
| Yellow Time (s) | 5.5 | 5.5 |  | 5.5 | 5.5 |  | 3.5 | 4.8 |  | 4.8 | 4.8 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 1.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 7.5 | 7.5 |  | 7.5 | 7.5 |  | 4.5 | 6.8 |  | 6.8 | 6.8 |  |
| Lead/Lag |  |  |  |  |  |  | Lead |  |  | Lag | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes |  |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | None | None |  | None | None |  |
| Act Effct Green (s) | 10.8 | 10.8 |  | 10.8 | 10.8 |  | 38.7 | 36.1 |  | 9.3 | 9.3 |  |
| Actuated g/C Ratio | 0.17 | 0.17 |  | 0.17 | 0.17 |  | 0.61 | 0.57 |  | 0.15 | 0.15 |  |
| v/c Ratio | 0.07 | 0.68 |  | 0.07 | 0.29 |  | 0.75 | 0.22 |  | 0.04 | 0.37 |  |
| Control Delay | 26.9 | 18.9 |  | 27.5 | 28.0 |  | 13.9 | 6.5 |  | 30.0 | 31.9 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 26.9 | 18.9 |  | 27.5 | 28.0 |  | 13.9 | 6.5 |  | 30.0 | 31.9 |  |
| LOS | C | B |  | C | C |  | B | A |  | C | C |  |
| Approach Delay |  | 19.3 |  |  | 27.9 |  |  | 12.0 |  |  | 31.8 |  |
| Approach LOS |  | B |  |  | C |  |  | B |  |  | C |  |
| Queue Length 50th (ft) | 6 | 39 |  | 3 | 33 |  | 118 | 32 |  | 3 | 37 |  |
| Queue Length 95th (ft) | 23 | 124 |  | 16 | 78 |  | 312 | 82 |  | 15 | 92 |  |
| Internal Link Dist (ft) |  | 897 |  |  | 1002 |  |  | 1518 |  |  | 1400 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 457 | 711 |  | 259 | 651 |  | 1146 | 1556 |  | 376 | 605 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.04 | 0.43 |  | 0.03 | 0.14 |  | 0.59 | 0.15 |  | 0.02 | 0.17 |  |

## Intersection Summary

```
Area Type: Other
```

Cycle Length: 90
Actuated Cycle Length: 63.2
Natural Cycle: 70
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.75
Intersection Signal Delay: 16.3
Intersection LOS: B
Intersection Capacity Utilization 69.8\%
ICU Level of Service C
Analysis Period (min) 15
Splits and Phases: 3:


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\hat{F}$ |  | ${ }^{7}$ | $\hat{F}$ |  | \% | $\hat{\square}$ |  | \% | $\uparrow$ |  |
| Traffic Volume (vph) | 12 | 67 | 628 | 13 | 77 | 7 | 215 | 93 | 7 | 4 | 162 | 10 |
| Future Volume (vph) | 12 | 67 | 628 | 13 | 77 | 7 | 215 | 93 | 7 | 4 | 162 | 10 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.864 |  |  | 0.987 |  |  | 0.989 |  |  | 0.991 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1770 | 1609 | 0 | 1770 | 1839 | 0 | 1770 | 1842 | 0 | 1770 | 1846 | 0 |
| Flt Permitted | 0.697 |  |  | 0.247 |  |  | 0.637 |  |  | 0.685 |  |  |
| Satd. Flow (perm) | 1298 | 1609 | 0 | 460 | 1839 | 0 | 1187 | 1842 | 0 | 1276 | 1846 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 567 |  |  | 8 |  |  | 7 |  |  | 6 |  |
| Link Speed (mph) |  | 55 |  |  | 55 |  |  | 45 |  |  | 45 |  |
| Link Distance (t) |  | 977 |  |  | 1082 |  |  | 1598 |  |  | 1480 |  |
| Travel Time (s) |  | 12.1 |  |  | 13.4 |  |  | 24.2 |  |  | 22.4 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% |
| Adj. Flow (vph) | 13 | 74 | 696 | 14 | 85 | 8 | 238 | 103 | 8 | 4 | 180 | 11 |


| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group Flow (vph) | 13 | 770 | 0 | 14 | 93 | 0 | 238 | 111 | 0 | 4 | 191 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(t) |  | 12 |  |  | 12 |  |  | 12 |  |  | 12 |  |
| Link Offset(ft) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(t) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 |  | 1 | 2 |  | 1 | 2 |  | 1 | 2 |  |
| Detector Template | Left | Thru |  | Left | Thru |  | Left | Thru |  | Left | Thru |  |
| Leading Detector (tt) | 20 | 100 |  | 20 | 100 |  | 20 | 100 |  | 20 | 100 |  |
| Trailing Detector (tt) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Position(ft) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Size(ft) | 20 | 6 |  | 20 | 6 |  | 20 | 6 |  | 20 | 6 |  |
| Detector 1 Type | Cl+Ex | Cl+Ex |  | Cl+Ex | Cl+Ex |  | Cl+Ex | Cl+Ex |  | Cl+Ex | Cl+Ex |  |


| Detector 1 Channel |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(tt) |  | 94 |  | 94 |  | 94 |  | 94 |
| Detector 2 Size(ft) |  | 6 |  | 6 |  | 6 |  | 6 |
| Detector 2 Type |  | Cl+Ex |  | Cl+Ex |  | Cl+Ex |  | Cl+Ex |

Detector 2 Channel

| Detector 2 Extend (s) |  | 0.0 |  | 0.0 |  | 0.0 |  | 0.0 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Turn Type | Perm | NA | Perm | NA | Perm | NA | Perm | NA |
| Protected Phases |  | 4 |  | 8 | 2 |  | 6 | 6 |
| Permitted Phases | 4 |  | 8 |  | 2 |  | 6 | 6 |

Switch Phase

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum Initial (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| Minimum Split (s) | 23.5 | 23.5 |  | 23.5 | 23.5 |  | 22.8 | 22.8 |  | 22.8 | 22.8 |  |
| Total Split (s) | 32.0 | 32.0 |  | 32.0 | 32.0 |  | 28.0 | 28.0 |  | 28.0 | 28.0 |  |
| Total Split (\%) | 53.3\% | 53.3\% |  | 53.3\% | 53.3\% |  | 46.7\% | 46.7\% |  | 46.7\% | 46.7\% |  |
| Maximum Green (s) | 24.5 | 24.5 |  | 24.5 | 24.5 |  | 21.2 | 21.2 |  | 21.2 | 21.2 |  |
| Yellow Time (s) | 5.5 | 5.5 |  | 5.5 | 5.5 |  | 4.8 | 4.8 |  | 4.8 | 4.8 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 7.5 | 7.5 |  | 7.5 | 7.5 |  | 6.8 | 6.8 |  | 6.8 | 6.8 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | None | None |  | None | None |  |
| Act Effct Green (s) | 20.8 | 20.8 |  | 20.8 | 20.8 |  | 15.3 | 15.3 |  | 14.7 | 14.7 |  |
| Actuated g/C Ratio | 0.50 | 0.50 |  | 0.50 | 0.50 |  | 0.36 | 0.36 |  | 0.35 | 0.35 |  |
| v/c Ratio | 0.02 | 0.71 |  | 0.06 | 0.10 |  | 0.55 | 0.16 |  | 0.01 | 0.29 |  |
| Control Delay | 10.4 | 8.8 |  | 11.5 | 10.1 |  | 20.0 | 12.7 |  | 12.5 | 13.9 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 10.4 | 8.8 |  | 11.5 | 10.1 |  | 20.0 | 12.7 |  | 12.5 | 13.9 |  |
| LOS | B | A |  | B | B |  | C | B |  | B | B |  |
| Approach Delay |  | 8.8 |  |  | 10.3 |  |  | 17.7 |  |  | 13.9 |  |
| Approach LOS |  | A |  |  | B |  |  | B |  |  | B |  |
| Queue Length 50th (ft) | 2 | 36 |  | 2 | 14 |  | 49 | 18 |  | 1 | 34 |  |
| Queue Length 95th (ft) | 11 | \#205 |  | 13 | 42 |  | 134 | 55 |  | 6 | 89 |  |
| Internal Link Dist (ft) |  | 897 |  |  | 1002 |  |  | 1518 |  |  | 1400 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 805 | 1213 |  | 285 | 1143 |  | 669 | 1041 |  | 719 | 1043 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.02 | 0.63 |  | 0.05 | 0.08 |  | 0.36 | 0.11 |  | 0.01 | 0.18 |  |

## Intersection Summary

```
Area Type: Other
```

Cycle Length: 60
Actuated Cycle Length: 42
Natural Cycle: 60
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.71
Intersection Signal Delay: 11.8
Intersection LOS: B
Intersection Capacity Utilization 82.2\%
ICU Level of Service E
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 3:


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Page 2

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{*}$ | $\dagger$ |  | ${ }^{*}$ | $\dagger$ |  | ${ }^{*}$ | $\dagger$ |  | ${ }^{*}$ | $\dagger$ |  |
| Traffic Volume (vph) | 17 | 70 | 281 | 10 | 96 | 9 | 764 | 245 | 17 | 7 | 100 | 16 |
| Future Volume (vph) | 17 | 70 | 281 | 10 | 96 | 9 | 764 | 245 | 17 | 7 | 100 | 16 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.880 |  |  | 0.987 |  |  | 0.990 |  |  | 0.979 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1770 | 1639 | 0 | 1770 | 1839 | 0 | 1770 | 1844 | 0 | 1770 | 1824 | 0 |
| Flt Permitted | 0.682 |  |  | 0.280 |  |  | 0.443 |  |  | 0.582 |  |  |
| Satd. Flow (perm) | 1270 | 1639 | 0 | 522 | 1839 | 0 | 825 | 1844 | 0 | 1084 | 1824 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 201 |  |  | 5 |  |  | 8 |  |  | 8 |  |
| Link Speed (mph) |  | 55 |  |  | 55 |  |  | 45 |  |  | 45 |  |
| Link Distance (ft) |  | 977 |  |  | 1082 |  |  | 1598 |  |  | 1480 |  |
| Travel Time (s) |  | 12.1 |  |  | 13.4 |  |  | 24.2 |  |  | 22.4 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Growth Factor | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% | 102\% |
| Adj. Flow (vph) | 19 | 78 | 312 | 11 | 106 | 10 | 847 | 272 | 19 | 8 | 111 | 18 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 19 | 390 | 0 | 11 | 116 | 0 | 847 | 291 | 0 | 8 | 129 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(ft) |  | 12 |  |  | 12 |  |  | 12 |  |  | 12 |  |
| Link Offset(ft) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(ft) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 |  | 1 | 2 |  | 1 | 2 |  | 1 | 2 |  |
| Detector Template | Left | Thru |  | Left | Thru |  | Left | Thru |  | Left | Thru |  |
| Leading Detector (ft) | 20 | 100 |  | 20 | 100 |  | 20 | 100 |  | 20 | 100 |  |
| Trailing Detector (ft) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Position(ft) | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Size(ft) | 20 | 6 |  | 20 | 6 |  | 20 | 6 |  | 20 | 6 |  |
| Detector 1 Type | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |  | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |  | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |  | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex |  |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 1 Queue (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 1 Delay (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 2 Position(ft) |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size(ft) |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | $\mathrm{Cl}+\mathrm{Ex}$ |  |  | $\mathrm{Cl}+\mathrm{Ex}$ |  |  | $\mathrm{Cl}+\mathrm{Ex}$ |  |  | $\mathrm{Cl}+\mathrm{Ex}$ |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | Perm | NA |  | Perm | NA |  | pm+pt | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 |  | 8 | 8 |  | 5 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum Initial (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 5.0 | 4.0 |  | 4.0 | 4.0 |  |
| Minimum Split (s) | 23.5 | 23.5 |  | 23.5 | 23.5 |  | 9.5 | 22.8 |  | 22.8 | 22.8 |  |
| Total Split (s) | 26.0 | 26.0 |  | 26.0 | 26.0 |  | 40.0 | 64.0 |  | 24.0 | 24.0 |  |
| Total Split (\%) | 28.9\% | 28.9\% |  | 28.9\% | 28.9\% |  | 44.4\% | 71.1\% |  | 26.7\% | 26.7\% |  |
| Maximum Green (s) | 18.5 | 18.5 |  | 18.5 | 18.5 |  | 35.5 | 57.2 |  | 17.2 | 17.2 |  |
| Yellow Time (s) | 5.5 | 5.5 |  | 5.5 | 5.5 |  | 3.5 | 4.8 |  | 4.8 | 4.8 |  |
| All-Red Time (s) | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 1.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 7.5 | 7.5 |  | 7.5 | 7.5 |  | 4.5 | 6.8 |  | 6.8 | 6.8 |  |
| Lead/Lag |  |  |  |  |  |  | Lead |  |  | Lag | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes |  |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None |  | None | None |  | None | None |  | None | None |  |
| Act Effct Green (s) | 14.3 | 14.3 |  | 14.3 | 14.3 |  | 48.4 | 45.9 |  | 10.7 | 10.7 |  |
| Actuated g/C Ratio | 0.19 | 0.19 |  | 0.19 | 0.19 |  | 0.64 | 0.61 |  | 0.14 | 0.14 |  |
| v/c Ratio | 0.08 | 0.82 |  | 0.11 | 0.33 |  | 0.88 | 0.26 |  | 0.05 | 0.49 |  |
| Control Delay | 28.4 | 31.1 |  | 30.8 | 30.5 |  | 23.7 | 7.4 |  | 31.7 | 37.8 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 28.4 | 31.1 |  | 30.8 | 30.5 |  | 23.7 | 7.4 |  | 31.7 | 37.8 |  |
| LOS | C | C |  | C | C |  | C | A |  | C | D |  |
| Approach Delay |  | 31.0 |  |  | 30.5 |  |  | 19.5 |  |  | 37.5 |  |
| Approach LOS |  | C |  |  | C |  |  | B |  |  | D |  |
| Queue Length 50th (ft) | 8 | 91 |  | 5 | 48 |  | 262 | 58 |  | 4 | 59 |  |
| Queue Length 95th (ft) | 27 | \#238 |  | 20 | 100 |  | \#553 | 100 |  | 16 | 113 |  |
| Internal Link Dist (ft) |  | 897 |  |  | 1002 |  |  | 1518 |  |  | 1400 |  |
| Turn Bay Length (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 329 | 574 |  | 135 | 481 |  | 1030 | 1395 |  | 261 | 446 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.06 | 0.68 |  | 0.08 | 0.24 |  | 0.82 | 0.21 |  | 0.03 | 0.29 |  |

## Intersection Summary

```
Area Type: Other
```

Cycle Length: 90
Actuated Cycle Length: 75.4
Natural Cycle: 90
Control Type: Actuated-Uncoordinated
Maximum v/c Ratio: 0.88
Intersection Signal Delay: 24.2
Intersection LOS: C
Intersection Capacity Utilization 83.2\%
ICU Level of Service E
Analysis Period (min) 15
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 3 :


Burgess\&Niple, Inc.

## MOVEMENT SUMMARY

## $\nabla$ Site: [AM - Opening (Site Folder: Opening)]

Culbreath Rd at Ayers Rd/Hayman Rd
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> mph |
| South: Culbreath Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 L2 | 170 | 3.0 | 185 | 3.0 | 0.218 | 4.8 | LOS A | 1.1 | 28.1 | 0.23 | 0.10 | 0.23 | 34.6 |
| 8 T1 | 74 | 3.0 | 80 | 3.0 | 0.218 | 4.8 | LOS A | 1.1 | 28.1 | 0.23 | 0.10 | 0.23 | 34.6 |
| 18 R2 | 6 | 3.0 | 7 | 3.0 | 0.218 | 4.8 | LOS A | 1.1 | 28.1 | 0.23 | 0.10 | 0.23 | 33.6 |
| Approach | 250 | 3.0 | 272 | 3.0 | 0.218 | 4.8 | LOS A | 1.1 | 28.1 | 0.23 | 0.10 | 0.23 | 34.6 |
| East: Hayman Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L 2 | 10 | 3.0 | 11 | 3.0 | 0.083 | 4.3 | LOS A | 0.3 | 8.9 | 0.41 | 0.28 | 0.41 | 38.6 |
| 6 T1 | 61 | 3.0 | 66 | 3.0 | 0.083 | 4.3 | LOS A | 0.3 | 8.9 | 0.41 | 0.28 | 0.41 | 38.5 |
| 16 R2 | 6 | 3.0 | 7 | 3.0 | 0.083 | 4.3 | LOS A | 0.3 | 8.9 | 0.41 | 0.28 | 0.41 | 37.3 |
| Approach | 77 | 3.0 | 84 | 3.0 | 0.083 | 4.3 | LOS A | 0.3 | 8.9 | 0.41 | 0.28 | 0.41 | 38.4 |
| North: Culbreath Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 3 | 3.0 | 3 | 3.0 | 0.150 | 4.9 | LOS A | 0.7 | 16.8 | 0.42 | 0.30 | 0.42 | 36.6 |
| 4 T1 | 129 | 3.0 | 140 | 3.0 | 0.150 | 4.9 | LOS A | 0.7 | 16.8 | 0.42 | 0.30 | 0.42 | 36.6 |
| 14 R2 | 8 | 3.0 | 9 | 3.0 | 0.150 | 4.9 | LOS A | 0.7 | 16.8 | 0.42 | 0.30 | 0.42 | 35.4 |
| Approach | 140 | 3.0 | 152 | 3.0 | 0.150 | 4.9 | LOS A | 0.7 | 16.8 | 0.42 | 0.30 | 0.42 | 36.5 |
| West: Ayers Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 L2 | 9 | 3.0 | 10 | 3.0 | 0.534 | 9.4 | LOS A | 3.8 | 97.4 | 0.51 | 0.34 | 0.51 | 35.8 |
| 2 T1 | 53 | 3.0 | 58 | 3.0 | 0.534 | 9.4 | LOS A | 3.8 | 97.4 | 0.51 | 0.34 | 0.51 | 35.8 |
| 12 R 2 | 498 | 3.0 | 541 | 3.0 | 0.534 | 9.4 | LOS A | 3.8 | 97.4 | 0.51 | 0.34 | 0.51 | 34.7 |
| Approach | 560 | 3.0 | 609 | 3.0 | 0.534 | 9.4 | LOS A | 3.8 | 97.4 | 0.51 | 0.34 | 0.51 | 34.8 |
| All Vehicles | 1027 | 3.0 | 1116 | 3.0 | 0.534 | 7.3 | LOS A | 3.8 | 97.4 | 0.42 | 0.27 | 0.42 | 35.2 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

## $\nexists$ Site: [PM - Opening (Site Folder: Opening)]

Culbreath Rd at Ayers Rd/Hayman Rd
Site Category: (None)
Roundabout


Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

## $\square$ Site: [AM - Future (Site Folder: Future)]

Culbreath Rd at Ayers Rd/Hayman Rd
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ | INPUT VOLUMES |  | DEMAND FLOWS |  | Deg. Satn <br> v/c | Aver. <br> Delay <br> sec | Level of Service | 95\% BACK OF QUEUE |  | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> mph |
| South: Culbreath Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 L2 | 215 | 3.0 | 234 | 3.0 | 0.281 | 5.5 | LOS A | 1.5 | 38.5 | 0.28 | 0.14 | 0.28 | 34.3 |
| 8 T1 | 93 | 3.0 | 101 | 3.0 | 0.281 | 5.5 | LOS A | 1.5 | 38.5 | 0.28 | 0.14 | 0.28 | 34.2 |
| 18 R2 | 7 | 3.0 | 8 | 3.0 | 0.281 | 5.5 | LOS A | 1.5 | 38.5 | 0.28 | 0.14 | 0.28 | 33.2 |
| Approach | 315 | 3.0 | 342 | 3.0 | 0.281 | 5.5 | LOS A | 1.5 | 38.5 | 0.28 | 0.14 | 0.28 | 34.2 |
| East: Hayman Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L 2 | 13 | 3.0 | 14 | 3.0 | 0.113 | 4.9 | LOS A | 0.5 | 12.1 | 0.47 | 0.36 | 0.47 | 38.2 |
| $6 \quad$ T1 | 77 | 3.0 | 84 | 3.0 | 0.113 | 4.9 | LOS A | 0.5 | 12.1 | 0.47 | 0.36 | 0.47 | 38.1 |
| 16 R 2 | 7 | 3.0 | 8 | 3.0 | 0.113 | 4.9 | LOS A | 0.5 | 12.1 | 0.47 | 0.36 | 0.47 | 36.9 |
| Approach | 97 | 3.0 | 105 | 3.0 | 0.113 | 4.9 | LOS A | 0.5 | 12.1 | 0.47 | 0.36 | 0.47 | 38.0 |
| North: Culbreath Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 4 | 3.0 | 4 | 3.0 | 0.202 | 5.8 | LOS A | 0.9 | 23.3 | 0.49 | 0.39 | 0.49 | 36.1 |
| 4 T1 | 162 | 3.0 | 176 | 3.0 | 0.202 | 5.8 | LOS A | 0.9 | 23.3 | 0.49 | 0.39 | 0.49 | 36.0 |
| 14 R2 | 10 | 3.0 | 11 | 3.0 | 0.202 | 5.8 | LOS A | 0.9 | 23.3 | 0.49 | 0.39 | 0.49 | 35.0 |
| Approach | 176 | 3.0 | 191 | 3.0 | 0.202 | 5.8 | LOS A | 0.9 | 23.3 | 0.49 | 0.39 | 0.49 | 36.0 |
| West: Ayers Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 L2 | 12 | 3.0 | 13 | 3.0 | 0.704 | 14.2 | LOS B | 10.7 | 274.3 | 0.72 | 0.65 | 1.00 | 33.2 |
| 2 T1 | 67 | 3.0 | 73 | 3.0 | 0.704 | 14.2 | LOS B | 10.7 | 274.3 | 0.72 | 0.65 | 1.00 | 33.2 |
| 12 R 2 | 628 | 3.0 | 683 | 3.0 | 0.704 | 14.2 | LOS B | 10.7 | 274.3 | 0.72 | 0.65 | 1.00 | 32.2 |
| Approach | 707 | 3.0 | 768 | 3.0 | 0.704 | 14.2 | LOS B | 10.7 | 274.3 | 0.72 | 0.65 | 1.00 | 32.3 |
| All Vehicles | 1295 | 3.0 | 1408 | 3.0 | 0.704 | 10.3 | LOS B | 10.7 | 274.3 | 0.56 | 0.47 | 0.71 | 33.7 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## MOVEMENT SUMMARY

$\square$ Site: [PM - Future (Site Folder: Future)]
Culbreath Rd at Ayers Rd/Hayman Rd
Site Category: (None)
Roundabout

| Vehicle Movement Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov Turn } \\ & \text { ID } \end{aligned}$ |  | $\begin{aligned} & \text { JT } \\ & \text { MES } \\ & \text { HV ] } \\ & \% \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { ND } \\ & \text { VS } \\ & \text { HV ] } \\ & \% \end{aligned}$ | Deg. Satn <br> v/c | Aver. Delay <br> sec | Level of Service | 95\% B <br> [ Veh. <br> veh | $\begin{aligned} & \text { CK OF } \\ & \text { UE } \\ & \text { Dist ] } \\ & \mathrm{ft} \end{aligned}$ | Prop. Que | Effective Stop Rate | Aver. No. Cycles | Aver. Speed <br> mph |
| South: Culbreath Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 L2 | 764 | 3.0 | 830 | 3.0 | 0.927 | 30.1 | LOS D | 37.9 | 970.2 | 1.00 | 0.79 | 1.40 | 25.0 |
| 8 T1 | 245 | 3.0 | 266 | 3.0 | 0.927 | 30.1 | LOS D | 37.9 | 970.2 | 1.00 | 0.79 | 1.40 | 25.0 |
| 18 R2 | 17 | 3.0 | 18 | 3.0 | 0.927 | 30.1 | LOS D | 37.9 | 970.2 | 1.00 | 0.79 | 1.40 | 24.5 |
| Approach | 1026 | 3.0 | 1115 | 3.0 | 0.927 | 30.1 | LOS D | 37.9 | 970.2 | 1.00 | 0.79 | 1.40 | 25.0 |
| East: Hayman Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1 L2 | 10 | 3.0 | 11 | 3.0 | 0.301 | 13.9 | LOS B | 1.2 | 30.4 | 0.76 | 0.78 | 0.87 | 33.3 |
| 6 T1 | 96 | 3.0 | 104 | 3.0 | 0.301 | 13.9 | LOS B | 1.2 | 30.4 | 0.76 | 0.78 | 0.87 | 33.3 |
| 16 R 2 | 9 | 3.0 | 10 | 3.0 | 0.301 | 13.9 | LOS B | 1.2 | 30.4 | 0.76 | 0.78 | 0.87 | 32.3 |
| Approach | 115 | 3.0 | 125 | 3.0 | 0.301 | 13.9 | LOS B | 1.2 | 30.4 | 0.76 | 0.78 | 0.87 | 33.2 |
| North: Culbreath Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 7 | 3.0 | 8 | 3.0 | 0.269 | 11.3 | LOS B | 1.0 | 26.8 | 0.71 | 0.71 | 0.71 | 33.1 |
| 4 T1 | 100 | 3.0 | 109 | 3.0 | 0.269 | 11.3 | LOS B | 1.0 | 26.8 | 0.71 | 0.71 | 0.71 | 33.1 |
| 14 R2 | 16 | 3.0 | 17 | 3.0 | 0.269 | 11.3 | LOS B | 1.0 | 26.8 | 0.71 | 0.71 | 0.71 | 32.1 |
| Approach | 123 | 3.0 | 134 | 3.0 | 0.269 | 11.3 | LOS B | 1.0 | 26.8 | 0.71 | 0.71 | 0.71 | 32.9 |
| West: Ayers Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 L2 | 17 | 3.0 | 18 | 3.0 | 0.341 | 6.4 | LOS A | 1.9 | 49.2 | 0.36 | 0.21 | 0.36 | 37.6 |
| 2 T1 | 70 | 3.0 | 76 | 3.0 | 0.341 | 6.4 | LOS A | 1.9 | 49.2 | 0.36 | 0.21 | 0.36 | 37.5 |
| 12 R 2 | 281 | 3.0 | 305 | 3.0 | 0.341 | 6.4 | LOS A | 1.9 | 49.2 | 0.36 | 0.21 | 0.36 | 36.3 |
| Approach | 368 | 3.0 | 400 | 3.0 | 0.341 | 6.4 | LOS A | 1.9 | 49.2 | 0.36 | 0.21 | 0.36 | 36.6 |
| All Vehicles | 1632 | 3.0 | 1774 | 3.0 | 0.927 | 22.2 | LOS C | 37.9 | 970.2 | 0.82 | 0.65 | 1.08 | 27.9 |

Site Level of Service (LOS) Method: Delay \& v/c (HCM 6). Site LOS Method is specified in the Parameter Settings dialog (Site tab).
Roundabout LOS Method: Same as Sign Control.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement.
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 6).
Roundabout Capacity Model: US HCM 6.
Delay Model: HCM Delay Formula (Geometric Delay is not included).
Queue Model: HCM Queue Formula.
Gap-Acceptance Capacity: Traditional M1.
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## APPENDIX D

Benefit Cost Analysis

| BCA Result Summary |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Factors |  | Alternative 1: Traffic Signal |  |  |  | Alternative 2: Roundabout |  |  |  |
|  |  |  | Undiscounted |  | Discounted to 2022\$ |  | Undiscounted |  | d to 2022\$ |
| Benefits |  |  |  |  |  |  |  |  |  |
| Delay Benefits |  | \$ | 949,161 | \$ | 658,477 | \$ | 1,134,344 | \$ | 798,736 |
| Safety Benefits |  | \$ | 7,500,984 | \$ | 4,466,244 | \$ | 10,569,568 | \$ | 6,293,344 |
|  | Total Benefits | \$ | 8,450,144 | \$ | 5,124,721 | \$ | 11,703,912 | \$ | 7,092,081 |
| Costs |  |  |  |  |  |  |  |  |  |
| Construction |  | \$ | 2,114,467 | \$ | 1,954,943 | \$ | 2,057,769 | \$ | 1,902,523 |
|  | Total Cost | \$ | 2,114,467 | \$ | 1,954,943 | \$ | 2,057,769 | \$ | 1,902,523 |
| Comparing Benefits to Costs |  |  |  |  |  |  |  |  |  |
| Net Present Value |  | \$ | 6,335,678 | \$ | 3,169,778 | \$ | 9,646,143 | \$ | 5,189,557 |
| Benefit-Cost Ratio |  |  | 4.00 |  | 2.62 |  | 5.69 |  | 3.73 |


| Assumptions |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Items |  | Value | Unit | Source |
| Travel Time Savings |  |  |  |  |
| Total Number of Workdays per year |  | 260 | day | 5 days per week |
| Average Vehicle Occupancy |  |  |  |  |
| Passenger Car |  | 1.48 | per vehicle | USDOT Grant BCA Guidance |
| Truck |  | 1 | per vehicle |  |
| Hourly Values of Travel Time Savings |  |  |  |  |
| All Purposes |  | 18.8 | \$ per person-hour | USDOT Grant BCA Guidance |
| Truck Drivers |  | 32.4 | \$ per person-hour |  |
| Safety Benefits |  |  |  |  |
| No Injury | \$ | 7,700 | \$ per crash |  |
| Possible Injury | \$ | 103,950 | \$ per crash |  |
| Non-incapacitating Injury | \$ | 180,180 | \$ per crash | (obtained by $6 / 12 / 23$ ) |
| Incapacitating Injury | \$ | 888,030 | \$ per crash |  |
| Killed | \$ | 10,890,000 | \$ per crash |  |
| Inflation Rate |  |  |  |  |
| Discount Rate |  | 4\% | per year | FDM Section 122.6 (obtained by 6/12/23) |


| Delay Reduction Benefits |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | Approach | Delay |  |  |  |  |  | Count Data |  |  |  |  |  |  |  |  |
|  |  | AM |  |  | PM |  |  | HV\% | Total |  | AM |  |  | PM |  |  |
|  |  | NB | TS | RA | NB | Ts | RA |  | AM | PM | 1 | T | R | 1 | T | R |
| 2025 | EB | 27.7 | 8.8 | ${ }^{9.4}$ | 51 | 19.3 | 5.4 | 2.60\% | 560 | 292 | 9 | 53 | 498 | 14 | 55 | 223 |
|  | WB | 27.5 | 10.3 | 4.3 | 51 | 27.9 | 9.3 | 3.60\% | 77 | 91 | 10 | 61 | 6 | 8 | 76 | 7 |
|  | NB | 5.4 | 17.7 | 4.8 | 7 | 12 | 13.6 | 2.70\% | 250 | 814 | 170 | 74 | 6 | 606 | 194 | 14 |
|  | SB | 0.2 | 13.9 | 4.9 | 0.5 | 31.8 | 8 | 2.70\% | 140 | 98 | 3 | 129 | 8 | 6 | 79 | 13 |
| 2035 | EB | 112 | 8.8 | 14.2 | 51 | 31 | 6.4 | 2.60\% | 707 | 368 | 12 | 67 | 628 | 17 | 70 | 281 |
|  | WB | 156.2 | 10.3 | 4.9 | 51 | 30.5 | 13.9 | 3.60\% | 97 | 115 | 13 | 77 | 7 | 10 | 96 | 9 |
|  | NB | 5.6 | 17.7 | 5.5 | 8.1 | 19.5 | 30.1 | 2.70\% | 315 | 1026 | 215 | 93 | 7 | 764 | 245 | 17 |
|  | SB | 0.2 | 13.9 | 5.8 | 0.4 | 37.5 | 11.3 | 2.70\% | 176 | 123 | 4 | 162 | 10 | 7 | 100 | 16 |


| Alternative 1: Traffic Signal |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | Approach | Benfit Per Hour |  |  |  |  |  |  |  | Travel Time Saving |  |  |  |  |  |  |  |  |  |  |
|  |  | AM |  |  |  | PM |  |  |  | AM |  |  |  | PM |  |  |  | Daily Saving |  | Annual Saving |
|  |  | PV |  | HV |  | PV |  | HV |  | PV |  | HV |  | PV |  | HV |  |  |  |  |
| 2025 | EB | \$ | 15,176 | \$ | 472 | \$ | 7,913 | \$ | 246 | \$ | 79.7 | \$ | 2.5 | \$ | 69.7 | \$ | 2.2 | 154.0 |  | $\$ \quad 22,482$ |
|  | wB | \$ | 2,065 | \$ | 90 | \$ | 2,441 | \$ | 106 | \$ | 9.9 | \$ | 0.4 | \$ | 15.7 | \$ | 0.7 | S | 26.6 |  |
|  | NB | \$ | 6,768 | \$ | 219 | \$ | 22,037 | \$ | 712 | \$ | (23.1) | \$ | (0.7) | \$ | (30.6) | \$ | (1.0) | \$ | (55.5) |  |
|  | SB | \$ | 3,790 | \$ | 122 | \$ | 2,653 | \$ | 86 | \$ | (14.4) | \$ | (0.5) | \$ | (23.1) | \$ | (0.7) | \$ | (38.7) |  |
| 2035 | EB | s | 19,160 | \$ | 596 | \$ | 9,973 | \$ | 310 | \$ | 549.3 | \$ | 17.1 | \$ | 55.4 | \$ | 1.7 | S | 623.5 |  |
|  | wB | \$ | 2,602 | \$ | 113 | \$ | 3,085 | \$ | 134 | \$ | 105.4 | \$ | 4.6 | \$ | 17.6 | \$ | 0.8 | \$ | 128.4 | ,93 |
|  | NB | \$ | 8,528 | \$ | 276 | , | 27,777 | \$ | 898 | \$ | (28.7) | \$ | (0.9) | \$ | (88.0) | \$ | (2.8) | \$ | (120.4) |  |
|  | SB | \$ | 4,765 | \$ | 154 | \$ | 3,330 | \$ | 108 | s | (18.1) | \$ | (0.6) | \$ | (34.3) | \$ | (1.1) |  | (54.1) |  |


| Alternative 2: Roundabout |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | Approach | Benfit Per Hour |  |  |  |  |  |  |  | AM |  |  |  | Travel Time Saving |  |  |  |  |  |  |
|  |  | AM |  |  |  | PM |  |  |  |  |  |  |  | PV ${ }^{\text {P }}$ |  | PM |  | Daily Saving |  | Annual Saving |
|  |  | PV |  | HV |  | PV |  | HV |  | PV |  | HV |  |  |  |  | - |  |  |  |
| 2025 | EB | \$$\$$$\$$$\$$ | 15,176 | \$ | 472 | \$ | 7,913 | \$ | 246 | \$ | 77.1 | \$ | 2.4 | \$ | 100.2 | \$ | 3.1 | \$ | 182.9 |  |
|  | WB |  | 2,065 | \$ | 90 | \$ | 2,441 | \$ | 106 | \$ | 13.3 | \$ | 0.6 | \$ | 28.3 | \$ | 1.2 | \$ | 43.4 | 45,482 |
|  | NB |  | 6,768 | \$ | 219 | \$ | 22,037 | \$ | 712 | \$ | 1.1 | \$ | 0.0 | \$ | (40.4) | \$ | (1.3) | \$ | (40.5) | 45,482 |
|  | SB |  | 3,790 | \$ | 122 | \$ | 2,653 | \$ | 86 | \$ | (4.9) | \$ | (0.2) | \$ | (5.5) | \$ | (0.2) | \$ | (10.8) |  |
| 2035 | EB | 5$\$$$\$$$\$$ | 19,160 | \$ | 596 | \$ | 9,973 | \$ | 310 | \$ | 520.5 | \$ | 16.2 | \$ | 123.6 | \$ | 3.8 | \$ | 664.1 |  |
|  | WB |  | 2,602 | \$ | 113 | \$ | 3,085 | \$ | 134 | \$ | 109.3 | \$ | 4.8 | \$ | 31.8 | \$ | 1.4 | \$ | 147.3 | \$ 160,762 |
|  | NB |  | 8,528 | \$ | 276 | \$ | 27,777 | \$ | 898 | \$ | 0.2 | \$ | 0.0 | \$ | (169.7) | s | (5.5) | \$ | (175.0) | \$ 100,762 |
|  | SB |  | 4,765 | \$ | 154 | \$ | 3,330 | \$ | 108 | \$ | (7.4) | \$ | (0.2) | \$ | (10.1) | \$ | (0.3) |  | (18.1) |  |


| Year | Alternative 1 |  |  |  | Alternative 2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Delay ReductionBenefits |  | Discounted to 2022\$ |  | Delay ReductionBenefits |  | Discounted to 20225 |  |
| 2025 | S | 22,482 | \$ | 19,98 |  | 82 | \$ | 40,43 |
| 2026 | s | 35,243 | \$ | 30,126 |  | 57,010 |  | 8,732 |
| 2027 |  | 8,004 | \$ | 39,456 |  | 8,538 |  | 56,333 |
| 2028 | s | 60,765 | \$ | 48,024 |  | 80,06 |  | 63,277 |
| 9 | \$ | 73,526 | \$ | 55,874 |  | 91,594 |  | 69,604 |
| 2030 |  | 86,287 | \$ | 63,049 |  | 103,12 |  | 75,35 |
| 2031 |  | 048 | \$ | 69,59 |  | 114,650 |  | 80,552 |
| 2032 |  | 111,810 | \$ | 75,534 |  | 126,178 |  | 85,242 |
| 33 |  | 124,571 | \$ | 80,919 |  | 137,706 |  | 89,451 |
| 2034 |  | 137,332 |  | 85,777 |  | 149,234 |  | 93,211 |
| 2035 | \$ | 150,093 | \$ | 90,142 | 5 | 160,762 |  | 96,55 |
| Total |  | 949,161 | \$ | 658 |  | 1,134,344 |  | 798,7 |

[^2]| Safety Benefits |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Year | Fatal | Incapacitating <br> Injury | Non- <br> incapacitating <br> Injury | Possible Injury | PDO | Total |  |
| 2016 | 0 | 1 | 0 | 0 | 1 | 2 |  |
| 2017 | 0 | 1 | 2 | 1 | 5 | 2 |  |
| 2018 | 0 | 2 | 3 | 0 | 6 | 11 |  |
| Grand Total | 0 | 4 | 5 | 1 | 12 | 22 |  |



| Year | Alternative 1 |  |  |  | Alternative 2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Safety Benefits |  | $\begin{gathered} \text { Discounted to } \\ 2022 \$ \\ \hline \end{gathered}$ |  | Safety Benefits |  | $\begin{gathered} \hline \text { Discounted to } \\ 2022 \$ \end{gathered}$ |  |
| 2025 | \$ | 681,908 | \$ | 556,640 | \$ | 960,870 | \$ | 784,356 |
| 2026 | \$ | 681,908 | \$ | 520,224 | \$ | 960,870 | \$ | 733,043 |
| 2027 |  | 681,908 | \$ | 486,191 | \$ | 960,870 | \$ | 685,087 |
| 2028 |  | 681,908 | \$ | 454,384 | \$ | 960,870 | \$ | 640,268 |
| 2029 | \$ | 681,908 | \$ | 424,658 | \$ | 960,870 | \$ | 598,381 |
| 2030 |  | 681,908 | \$ | 396,876 | \$ | 960,870 | \$ | 559,235 |
| 2031 | \$ | 681,908 | \$ | 370,913 | \$ | 960,870 | \$ | 522,650 |
| 2032 | \$ | 681,908 | \$ | 346,647 | \$ | 960,870 | \$ | 488,457 |
| 2033 | \$ | 681,908 | \$ | 323,969 | \$ | 960,870 | \$ | 456,502 |
| 2034 | \$ | 681,908 | \$ | 302,775 | \$ | 960,870 | \$ | 426,638 |
| 2035 |  | 681,908 | \$ | 282,967 | \$ | 960,870 | \$ | 398,727 |
|  |  | 7,500,984 | \$ | 4,466,244 | \$ | 10,569,568 | \$ | 6,293,344 |


|  | Data Input |
| :--- | :--- |
|  | Description |
| Intermediate Calculation Results |  |
| Subtotal Calculation Results |  |

## ENGINEER'S ESTIMATE

## HERNANDO COUNTY

FINANCIAL PROJECT ID \# :


COMPONENT GROUPS

| 100 - STRUCTURES NOT USED |  |
| :---: | :---: |
| 200-ROADWAY | \$1,132,450.17 |
| 300 - SIGNING \& PAVEMENT MARKINGS | \$25,950.80 |
| 400 - LIGHTING NOT USED |  |
| 500 - SIGNALIZATION | \$333,490.25 |
| 550 - ITS NOT USED |  |
| 600 - LANDSCAPE / PERIPHERALS NOT USED |  |
| 700 - UTILITIES NOT USED |  |
| 800 - ARCHITECTURAL NOT USED |  |
| 900 - MASS TRANSIT NOT USED |  |
| 1000 - INVALID \& OTHER ITEMS NOT USED |  |
| COMPONENT SUB-TOTAL | \$1,491,891.22 |
| (102-1) MOT (Maintenance of Traffic) $10 \%$ | \$149,189.12 |
| SUB-TOTAL | \$1,641,080.34 |
| (101-1) MOB (Mobilization) 10\% | \$164,108.03 |
| SUB-TOTAL | \$1,805,188.37 |
| PU (Project Unknowns) 15\% | \$270,778.26 |
| SUB-TOTAL | \$2,075,966.63 |
| (999-25) Initial Contingency (Do Not Bid) | \$38,500.00 |
| PROJECT GRAND TOTAL | \$2,114,466.63 |

NOTES:
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## ENGINEER'S ESTIMATE

HILLSBOROUGH COUNTY

FINANCIAL PROJECT ID:
FILE VERSION PAGE NUMBER

## 200-Roadway

| PAY ITEM \# | ITEM DESCRIPTION | UNIT | QUANTITY | UNIT COST | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 01011 | MOBILIZATION |  | 10\% | See Summary Sheet |  |
| 01021 | MAINTENANCE OF TRAFFIC |  | 10\% | See Summary Sheet |  |
| 011011 | CLEARING \& GRUBBING | AC | 5.0 | \$54,807.65 | \$274,038.25 |
| 0110410 | REMOVAL OF EXISTING CONCRETE | SY | 1400 | \$35.11 | \$49,154.00 |
| 01604 | TYPE B STABILIZATION | SY | 10262 | \$8.43 | \$86,508.66 |
| 0285709 | OPTIONAL BASE, BASE GROUP 09 | SY | 3840 | \$22.78 | \$87,475.20 |
| 0327706 | MILLING EXIST ASPH PAVT, 1 1/2" AVG DEPTH | SY | 9111 | \$3.68 | \$33,528.48 |
| 0334153 | SUPERPAVE ASPHALTIC CONCRETE, TRAFFIC C, PG76-22 | TN | 634 | \$155.36 | \$98,498.24 |
| 0337783 | ASPHALT CONCRETE FRICTION COURSE,TRAFFIC C, FC-12.5, PG 76-22 | TN | 1069 | \$152.04 | \$162,530.76 |
| 0430175136 | PIPE CULVERT, OPT MATERIAL, ROUND, 36"S/CD | LF | 300 | \$252.82 | \$75,846.00 |
| 0430982138 | MITERED END SECTION, OPTIONAL ROUND, 36" CD | EA | 6 | \$8,015.00 | \$48,090.00 |
| 052411 | CONCRETE DITCH PAVT, NON REINFORCED, 3' | SY | 1400 | \$74.27 | \$103,978.00 |
| 057012 | PERFORMANCE TURF, SOD | SY | 22293 | \$5.06 | \$112,802.58 |
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|  |  |  |  |  |  |
| 200-Roadway |  | COMPONENT TOTAL |  |  | \$1,132,450.17 |

## ENGINEER'S ESTIMATE

## HILLSBOROGH COUNTY

## 300-Signing \& Pavement Markings

|  |  |
| ---: | :---: |
| FINANCIAL PROJECT ID: |  |
| FILE VERSION: | EE_01-27_Rev30 |
| PAGE NUMBER: | 3 of 3 |


| PAY ITEM \# | ITEM DESCRIPTION | UNIT | QUANTITY | UNIT COST | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0700111 | SINGLE POST SIGN, F\&I GROUND MOUNT, UP TO 12 SF | AS |  | \$457.35 | \$457.35 |
| 0700160 | SINGLE POST SIGN, REMOVE | AS | 14 | \$45.37 | \$635.18 |
| 071111125 | THERMOPLASTIC, STANDARD, WHITE, SOLID, 24" FOR STOP LINE AND CROSSWALK | LF | 96 | \$4.07 | \$390.72 |
| 071115101 | THERMOPLASTIC, STANDARD-OPEN GRADED ASPHALT SURFACES WHITE, SOLID, 6 " ${ }^{\text {² }}$ | GM | 1.66 | \$6,113.26 | \$10,148.01 |
| 071111170 | THERMOPLASTIC, STANDARD, WHITE, ARROW | EA | 19 | \$69.13 | \$1,313.47 |
| 071115201 | THERMOPLASTIC, STANDARD-OPEN GRADED ASPHALT SURFACES, YELLOW, SOLID, 6" | GM | 1.86 | \$6,113.26 | \$11,370.66 |
| 071111224 | THERMOPLASTIC, STANDARD, YELLOW, SOLID, 18" FOR DIAGONAL OR CHEVRON | LF | 340 | \$4.81 | \$1,635.40 |
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| 300-Signing | \& Pavement Markings |  | COMPONENT | TOTAL | \$25,950.80 |

# ENGINEER'S ESTIMATE FLORIDA DEPARTMENT OF TRANSPORTATION DISTRICT 7 

FINANCIAL PROJECT ID: FILE VERSION: PAGE NUMBER


## 500-Signalization

| PAY ITEM \# | ITEM DESCRIPTION | UNIT | QUANTITY | UNIT COST | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0630211 | CONDUIT, FURNISH \& INSTALL, OPEN TRENCH | LF | 85 | \$17.05 | \$1,449.25 |
| 0630212 | CONDUIT, FURNISH \& INSTALL, DIRECTIONAL BORE | LF | 511 | \$35.35 | \$18,063.85 |
| 063271 | SIGNAL CABLE- NEW OR RECONSTRUCTED INTERSECTION, FURNISH \& INSTALL | PI | 1 | \$9,675.05 | \$9,675.05 |
| 06331121 | FIBER OPTIC CABLE, F\&I, UNDERGROUND, 2-12 FIBERS | LF | 220 | \$3.93 | \$864.60 |
| 0633231 | FIBER OPTIC CONNECTION, INSTALL, SPLICE | EA | 12 | \$54.05 | \$648.60 |
| 0633232 | FIBER OPTIC CONNECTION, INSTALL, TERMINATION | EA | 12 | \$103.45 | \$1,241.40 |
| 0633311 | FIBER OPTIC CONNECTION HARDWARE, F\&I, SPLICE ENCLOSURE | EA | 1 | \$1,251.40 | \$1,251.40 |
| 0633312 | FIBER OPTIC CONNECTION HARDWARE, F\&I, SPLICE TRAY | EA | 1 | \$153.97 | \$153.97 |
| 0633314 | FIBER OPTIC CONNECTION HARDWARE, F\&I, BUFFER TUBE FAN OUT KIT | EA | 1 | \$93.78 | \$93.78 |
| 0633315 | FIBER OPTIC CONNECTION HARDWARE, F\&I, PRETERMINATED PATCH PANEL | EA | 1 | \$1,580.44 | \$1,580.44 |
| 0635211 | PULL \& SPLICE BOX, F\&I, 13 " $\times 24$ " COVER SIZE | EA | 16 | \$1,397.09 | \$22,353.44 |
| 0635213 | PULL \& SPLICE BOX, F\&I, 30" $\times 60$ " RECTANGULAR OR 36" ROUND COVER SIZE | EA | 1 | \$5,831.30 | \$5,831.30 |
| 06391122 | ELECTRICAL POWER SERVICE, F\&I, UNDERGROUND, METER PURCHASED BY CON | AS | 1 | \$4,585.66 | \$4,585.66 |
| 063921 | ELECTRICAL SERVICE WIRE, FURNISH \& INSTALL | LF | 20 | \$18.79 | \$375.80 |
| 0641212 | PRESTRESSED CONCRETE POLE, F\&I, TYPE P-II SERVICE POLE | EA | 1 | \$1,849.04 | \$1,849.04 |
| 0641218 | PRESTRESSED CONCRETE POLE, F\&I, TYPE P-VIII | EA | 4 | \$19,733.64 | \$78,934.56 |
| 0646111 | ALUMINUM SIGNALS POLE, PEDESTAL | EA | 8 | \$2,410.94 | \$19,287.52 |
| 0650114 | VEHICULAR TRAFFIC SIGNAL, FURNISH \& INSTALL ALUMINUM, 3 SECTION, 1 WAY | AS | 4 | \$1,755.30 | \$7,021.20 |
| 0650116 | VEHICULAR TRAFFIC SIGNAL, FURNISH \& INSTALL ALUMINUM, 4 SECTION, 1 WAY | AS | 4 | \$1,698.21 | \$6,792.84 |
| 0653111 | SIGNAL PEDESTRIAN, 12 INCH, INCANDESCENT, 1 WAY | AS | 8 | \$810.03 | \$6,480.24 |
| 0660411 | VEHICLE DETECTION SYSTEM- VIDEO, FURNISH \& INSTALL CABINET EQUIPMENT | EA | 1 | \$20,547.77 | \$20,547.77 |
| 0660412 | VEHICLE DETECTION SYSTEM- VIDEO, FURNISH \& INSTALL ABOVE GROUND EQUIF | EA | 4 | \$6,892.29 | \$27,569.16 |
| 06631111 | SIGNAL PRIORITY AND PREEMPTION SYSTEM, F\&I, OPTICAL, CABINET ELECTRON | EA | 1 | \$7,166.97 | \$7,166.97 |
| 06631112 | SIGNAL PRIORITY AND PREEMPTION SYSTEM, F\&I, OPTICAL, DETECTOR | EA | 2 | \$3,550.78 | \$7,101.56 |
| 0665111 | PEDESTRIAN DETECTOR, FURNISH \& INSTALL, STANDARD | EA | 8 | \$309.36 | \$2,474.88 |
| 06705111 | TRAFFIC CONTROLLER ASSEMBLY, F\&I, NEMA, 1 PREEMPTION | AS | 1 | \$42,473.60 | \$42,473.60 |
| 068411 | MANAGED FIELD ETHERNET SWITCH, FURNISH \& INSTALL | EA | 1 | \$5,041.64 | \$5,041.64 |
| 0685114 | UNINTERRUPTIBLE POWER SUPPLY, FURNISH AND INSTALL, ONLINE/DOUBLE CON | EA | 1 | \$13,331.93 | \$13,331.93 |
| 0700522 | INTERNALLY ILLUMINATED SIGN, FURNISH \& INSTALL, OVERHEAD MOUNT, 12-18 S | EA | 4 | \$4,812.20 | \$19,248.80 |
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| 500-Signalization |  | COMPONENT TOTAL |  |  | \$333,490.25 |

## ENGINEER'S ESTIMATE

## HERNANDO COUNTY

FINANCIAL PROJECT ID \# :


COMPONENT GROUPS

| 100 - STRUCTURES NOT USED |  |
| :---: | :---: |
| 200 - ROADWAY | \$1,262,766.01 |
| 300 - SIGNING \& PAVEMENT MARKINGS | \$12,025.19 |
| 400 - LIGHTING NOT USED |  |
| 500 - SIGNALIZATION NOT USED |  |
| 550 - ITS NOT USED |  |
| 600 - LANDSCAPE / PERIPHERALS NOT USED |  |
| 700 - UTILITIES NOT USED |  |
| 800 - ARCHITECTURAL NOT USED |  |
| 900 - MASS TRANSIT NOT USED |  |
| 1000 - INVALID \& OTHER ITEMS NOT USED |  |
| COMPONENT SUB-TOTAL | \$1,274,791.20 |
| (102-1) MOT (Maintenance of Traffic) $20 \%$ | \$254,958.24 |
| SUB-TOTAL | \$1,529,749.43 |
| (101-1) MOB (Mobilization) 10\% | \$152,974.94 |
| SUB-TOTAL | \$1,682,724.38 |
| PU (Project Unknowns) 20\% | \$336,544.88 |
| SUB-TOTAL | \$2,019,269.25 |
| (999-25) Initial Contingency (Do Not Bid) | \$38,500.00 |
| PROJECT GRAND TOTAL | \$2,057,769.25 |

NOTES:
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## ENGINEER'S ESTIMATE

HILLSBOROUGH COUNTY

FINANCIAL PROJECT ID:
FILE VERSION PAGE NUMBER

EE_01-27 Rev30 2 of 3

## 200-Roadway

| PAY ITEM \# | ITEM DESCRIPTION | UNIT | QUANTITY | UNIT COST | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 01011 | MOBILIZATION |  | 10\% | See Summary Sheet |  |
| 01021 | MAINTENANCE OF TRAFFIC |  | 20\% | See Summary Sheet |  |
| 011011 | CLEARING \& GRUBBING | AC | 3.7 | \$54,807.65 | \$202,788.31 |
| 0110410 | REMOVAL OF EXISTING CONCRETE | SY | 1245 | \$35.11 | \$43,711.95 |
| 01604 | TYPE B STABILIZATION | SY | 8744 | \$8.43 | \$73,711.92 |
| 0285709 | OPTIONAL BASE, BASE GROUP 09 | SY | 5762 | \$22.78 | \$131,258.36 |
| 0334153 | SUPERPAVE ASPHALTIC CONCRETE, TRAFFIC C, PG76-22 | TN | 951 | \$155.36 | \$147,747.36 |
| 0337783 | ASPHALT CONCRETE FRICTION COURSE,TRAFFIC C, FC-12.5, PG 76-22 | TN | 476 | \$152.04 | \$72,371.04 |
| 03503013 | CONCRETE PAVEMENT FOR ROUNDABOUT APRON, 12" DEPTH | SY | 313 | \$136.35 | \$42,677.55 |
| 04251461 | INLETS, CURB, TYPE J-6, <10' | EA | 4 | \$10,699.32 | \$42,797.28 |
| 04251541 | INLETS, DT BOT, TYPE D, <10' | EA | 4 | \$7,429.41 | \$29,717.64 |
| 0430175118 | PIPE CULVERT,OPTIONAL MATERIAL,ROUND, 18"S/CD | LF | 350 | \$134.39 | \$47,036.50 |
| 0430175136 | PIPE CULVERT, OPT MATERIAL, ROUND, 36"S/CD | LF | 570 | \$252.82 | \$144,107.40 |
| 0430982138 | MITERED END SECTION, OPTIONAL ROUND, 36" CD | EA | 6 | \$8,015.00 | \$48,090.00 |
| 052017 | CONCRETE CURB \& GUTTER, TYPE E | LF | 1716 | \$34.59 | \$59,356.44 |
| 0520110 | CONCRETE CURB \& GUTTER, TYPE F | LF | 772 | \$60.65 | \$46,821.80 |
| 052024 | CONCRETE CURB, TYPE D | LF | 250 | \$50.66 | \$12,665.00 |
| 052028 | CONCRETE CURB, TYPE RA | LF | 327 | \$56.46 | \$18,462.42 |
| 052411 | CONCRETE DITCH PAVT, NON REINFORCED, 3' | SY | 670 | \$74.27 | \$49,760.90 |
| 057012 | PERFORMANCE TURF, SOD | SY | 9819 | \$5.06 | \$49,684.14 |
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| 200-Roadw |  | COMPONENT TOTAL |  |  | \$1,262,766.01 |

## ENGINEER'S ESTIMATE

## HILLSBOROGH COUNTY

## 300-Signing \& Pavement Markings

| FINANCIAL PROJECT ID: |  |
| ---: | :--- |
| FILE VERSION: |  |
| PAGE NUMBER: | EE_01-27_Rev30 |
| 3 |  |


| PAY ITEM \# | ITEM DESCRIPTION | UNIT | QUANTITY | UNIT COST | TOTAL COST |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0700111 | SINGLE POST SIGN, F\&I GROUND MOUNT, UP TO 12 SF | AS |  | \$457.35 | \$457.35 |
| 0700160 | SINGLE POST SIGN, REMOVE | AS | 14 | \$45.37 | \$635.18 |
| 071111123 | THERMOPLASTIC, STANDARD, WHITE, SOLID, 12" FOR CROSSWALK AND ROUNDABOUT | LF | 65 | \$4.07 | \$264.55 |
| 071115101 | THERMOPLASTIC, STANDARD-OPEN GRADED ASPHALT SURFACES WHITE, SOLID, 6 " ${ }^{\prime \prime}$ | GM | 0.63 | \$6,113.26 | \$3,851.35 |
| 071111160 | THERMOPLASTIC, STANDARD, WHITE, MESSAGE OR SYMBOL | EA | 4 | \$247.09 | \$988.36 |
| 071115201 | THERMOPLASTIC, STANDARD-OPEN GRADED ASPHALT SURFACES, YELLOW, SOLID, 6" | GM | 0.87 | \$6,113.26 | \$5,318.54 |
| 071111224 | THERMOPLASTIC, STANDARD, YELLOW, SOLID, 18" FOR DIAGONAL OR CHEVRON | LF | 106 | \$4.81 | \$509.86 |
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| 300-Signing | \& Pavement Markings |  | COMPONENT | TOTAL | \$12,025.19 |


[^0]:    Note: NA* stop control delay and LOS is not available due to the volumes exceed modeled capacity in Synchro.

[^1]:    * Note: 93 pph applies as the lower threshold volume

[^2]:    Data Input
    Description
    Intermediate Calculation Results
    Subtotal Calculation Results

